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Citation:

Miles-Shenton, D (2013) Closing the Performance Gap: Beyond Stamford Brook. In: Better Building International Conference for a Sustainable Built Environment, 24th April 2013, Croke Park, Dublin. (Unpublished)

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24th April 2013, Croke Park, Dublin

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International Conference for  
a Sustainable Built Environment



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# Closing the Performance Gap: Beyond Stamford Brook

**Dominic Miles-Shenton**

David Johnston, Jez Wingfield, David Farmer, Malcolm Bell

# Closing the Performance Gap: Beyond Stamford Brook

Evidence of a Fabric Performance Gap?

How can it be Measured?

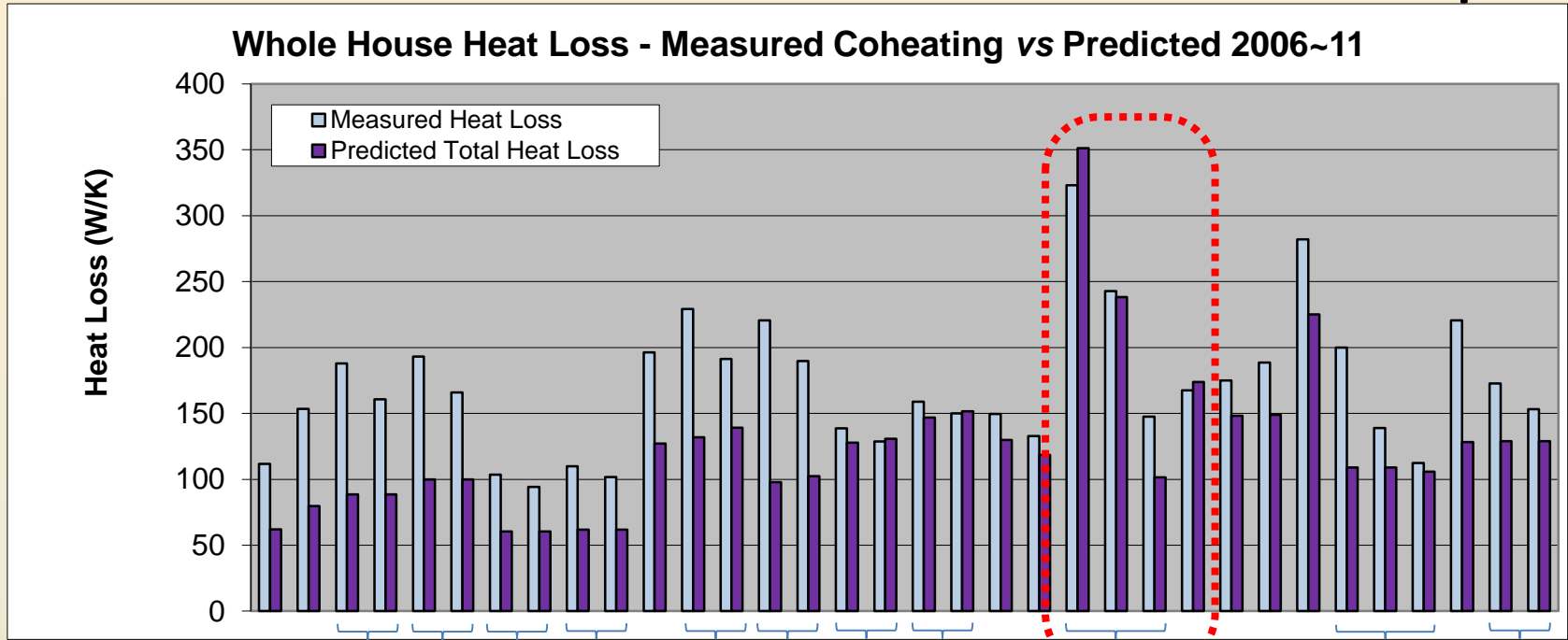
Regulatory Implications – so far...

Performance Gap for Retrofit

Closing the Loop

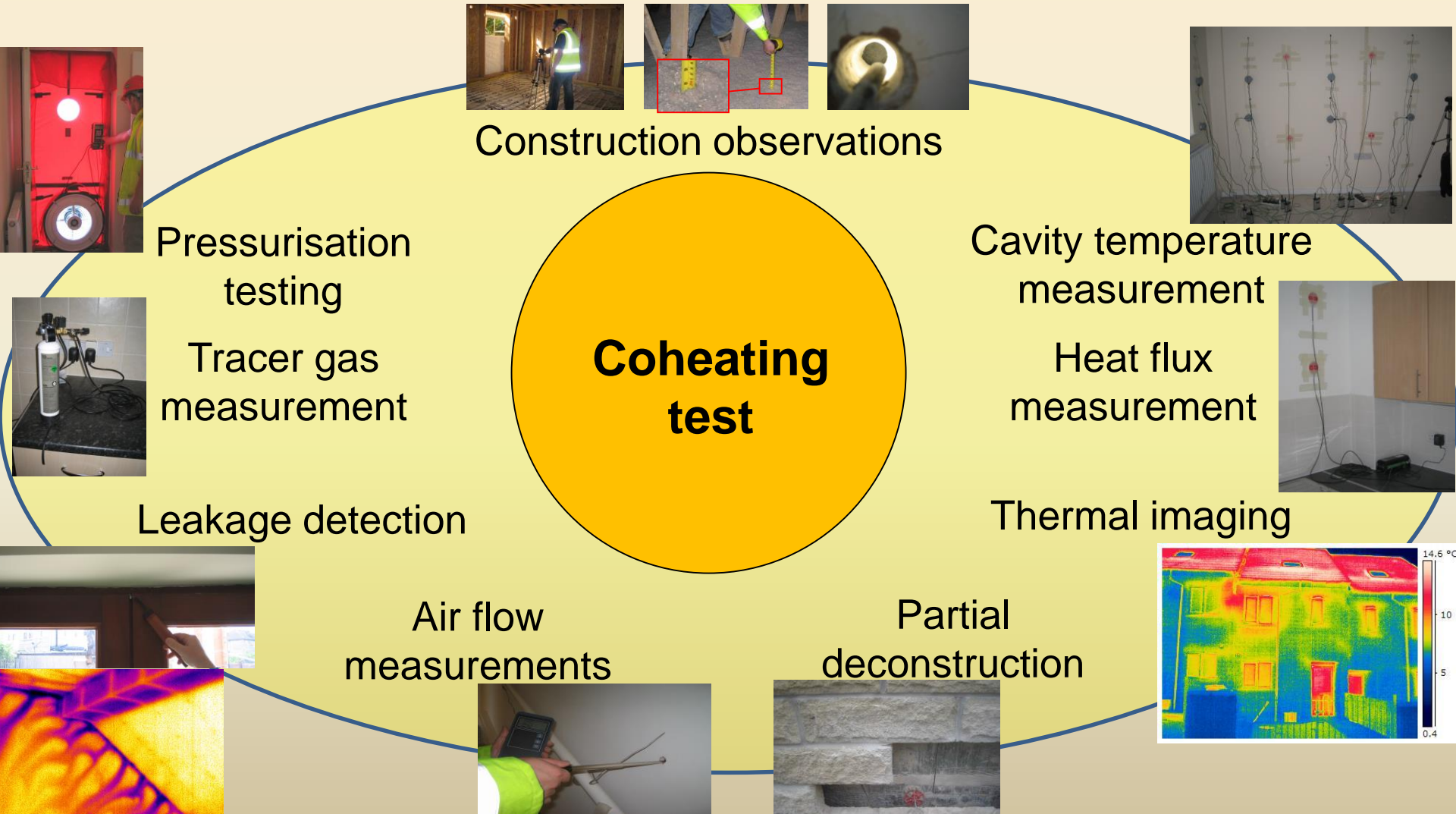
Simple Tests (do try this at home!)

# Evidence for a fabric Performance Gap



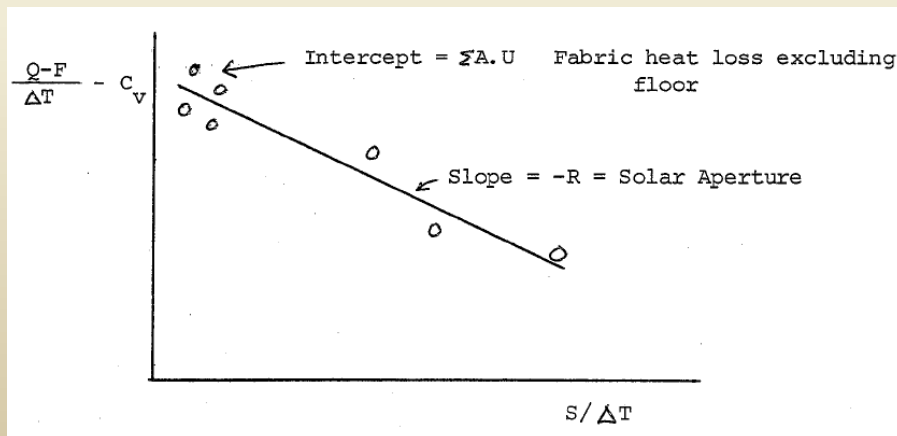
- The performance of the building fabric performance is very rarely understood and often taken for granted.
- Heat loss is often much higher than calculated during design.
- Highly dependent upon the design and installation of the insulation layers (Hens et al., 2007 and Doran, 2000).

# Measuring the Performance Gap



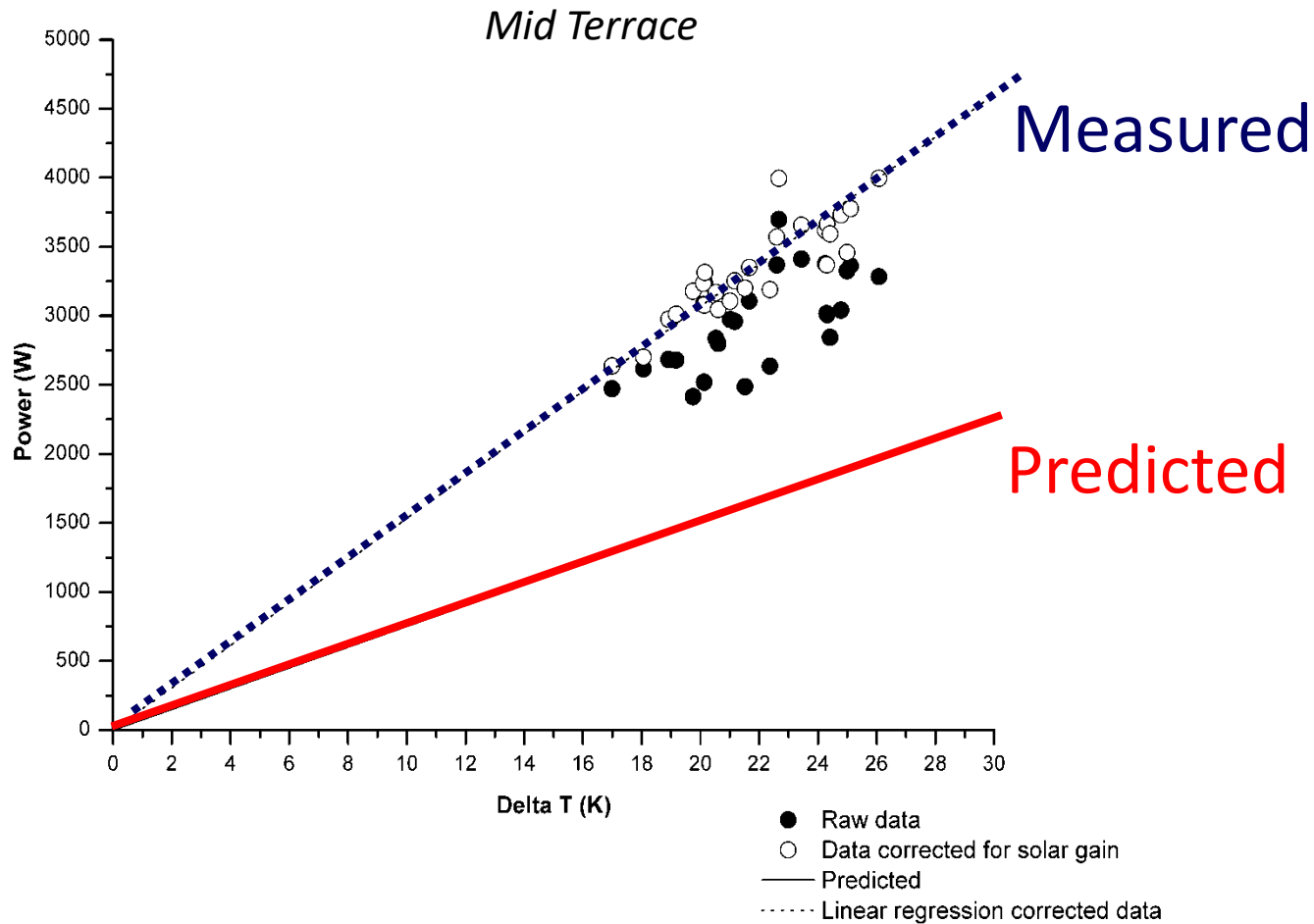
# Coheating Testing

- It is **NOT** a new concept, although it is in its infancy.
- Developed in the USA (LBL) in the late 1970's in response to the energy crisis (see Sonderegger et al. 1979).
- Used in a small number of occasions in the UK in the 1980's.
- Re-invented by Leeds Met at Stamford Brook 2005/6

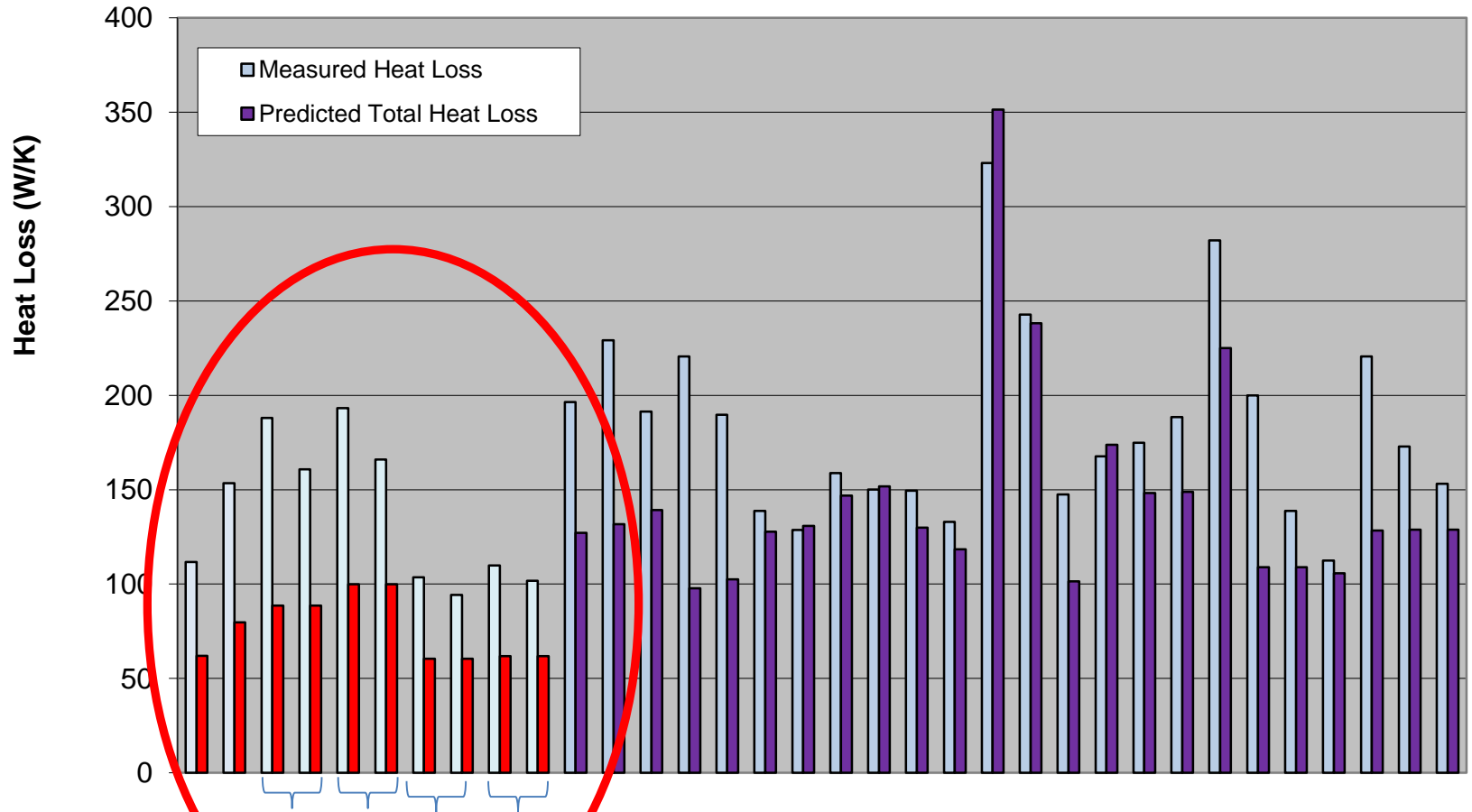


Sivour Analysis:  
(solar/ $\Delta T$ ) vs. (power/ $\Delta T$ )  
Heat Loss = y intercept  
Solar Aperture = slope

# Coheating Testing



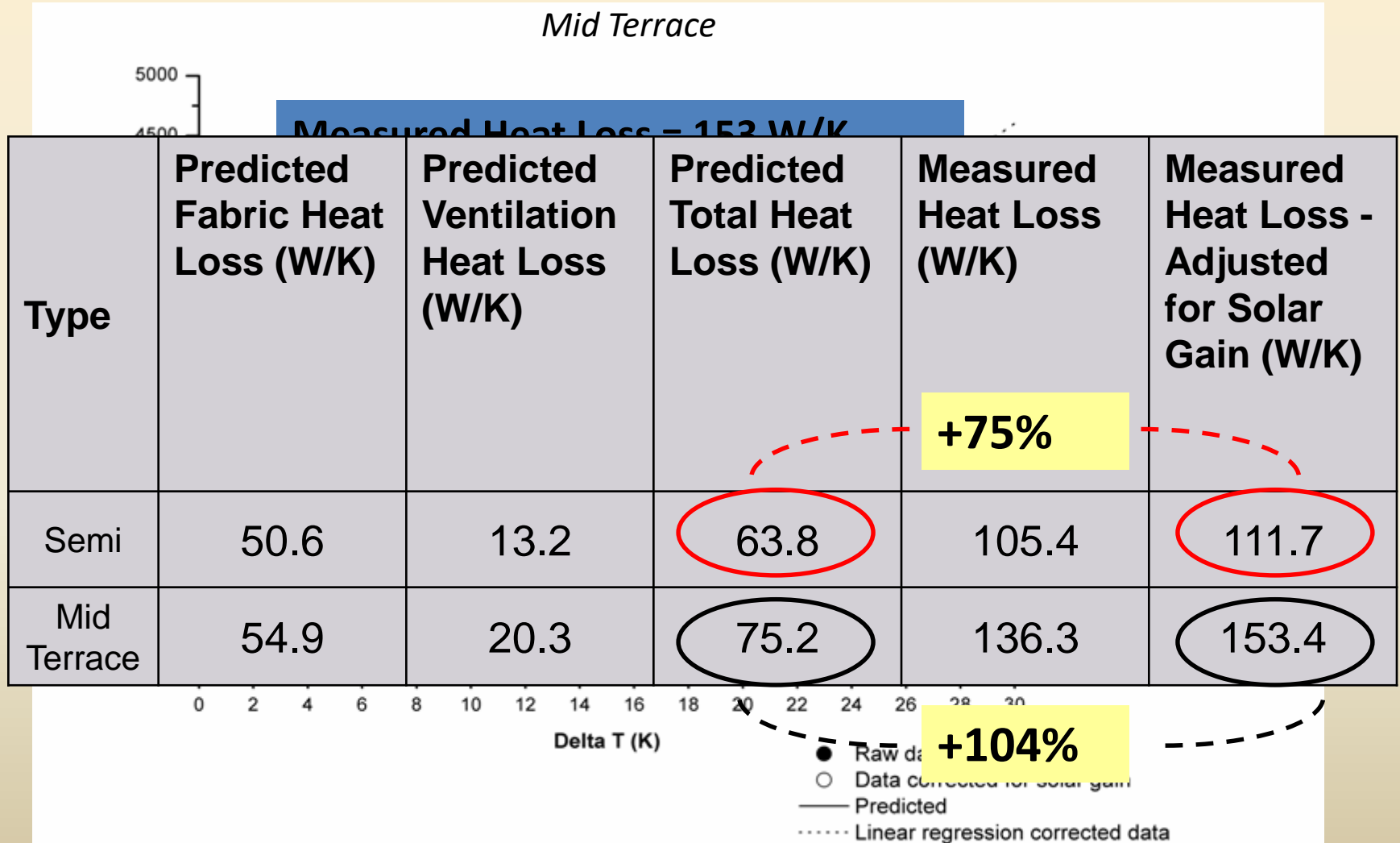
## Whole House Heat Loss - Measured Coheating versus Predicted



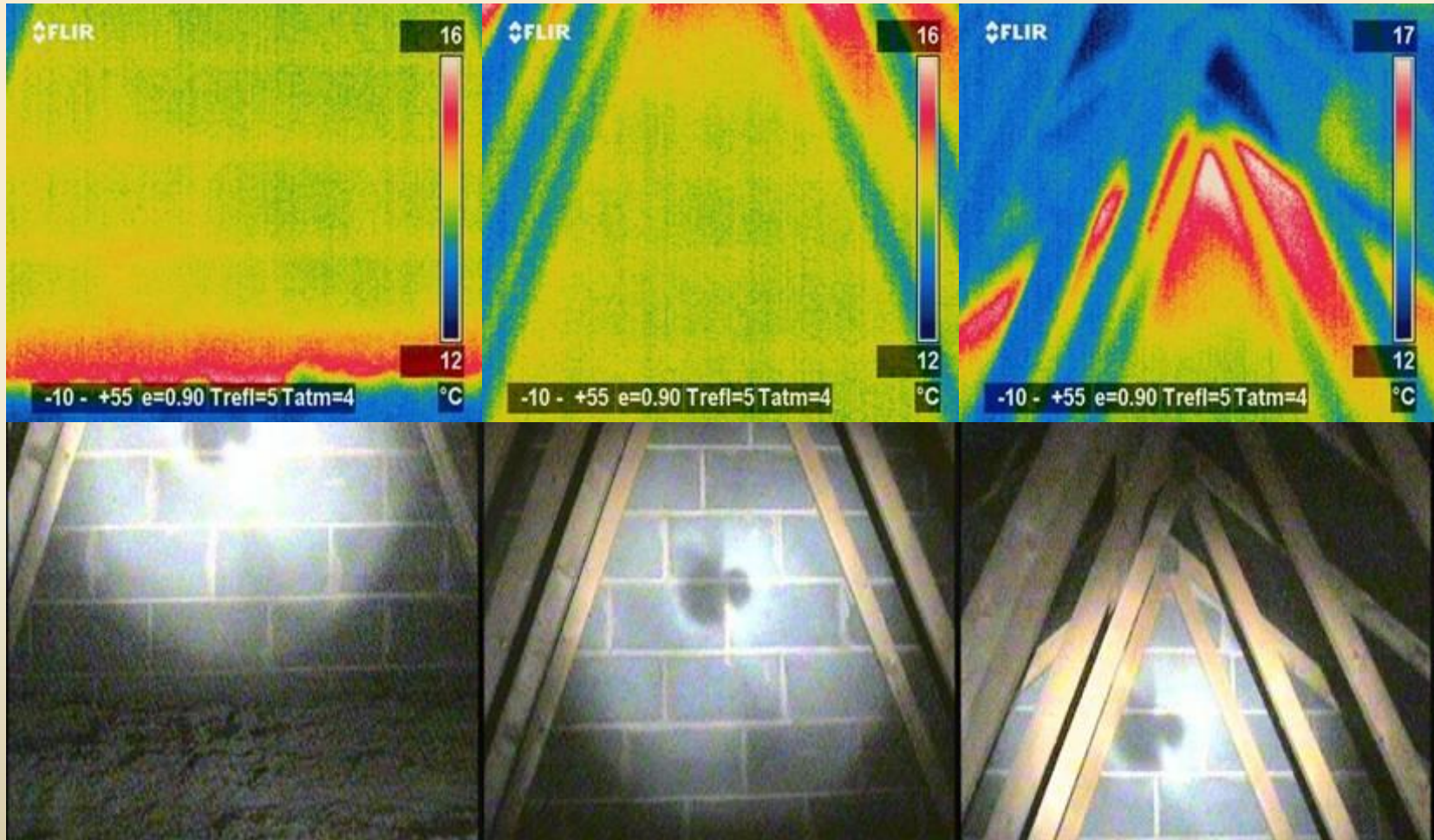
Party wall bypass investigations – Stamford Brook



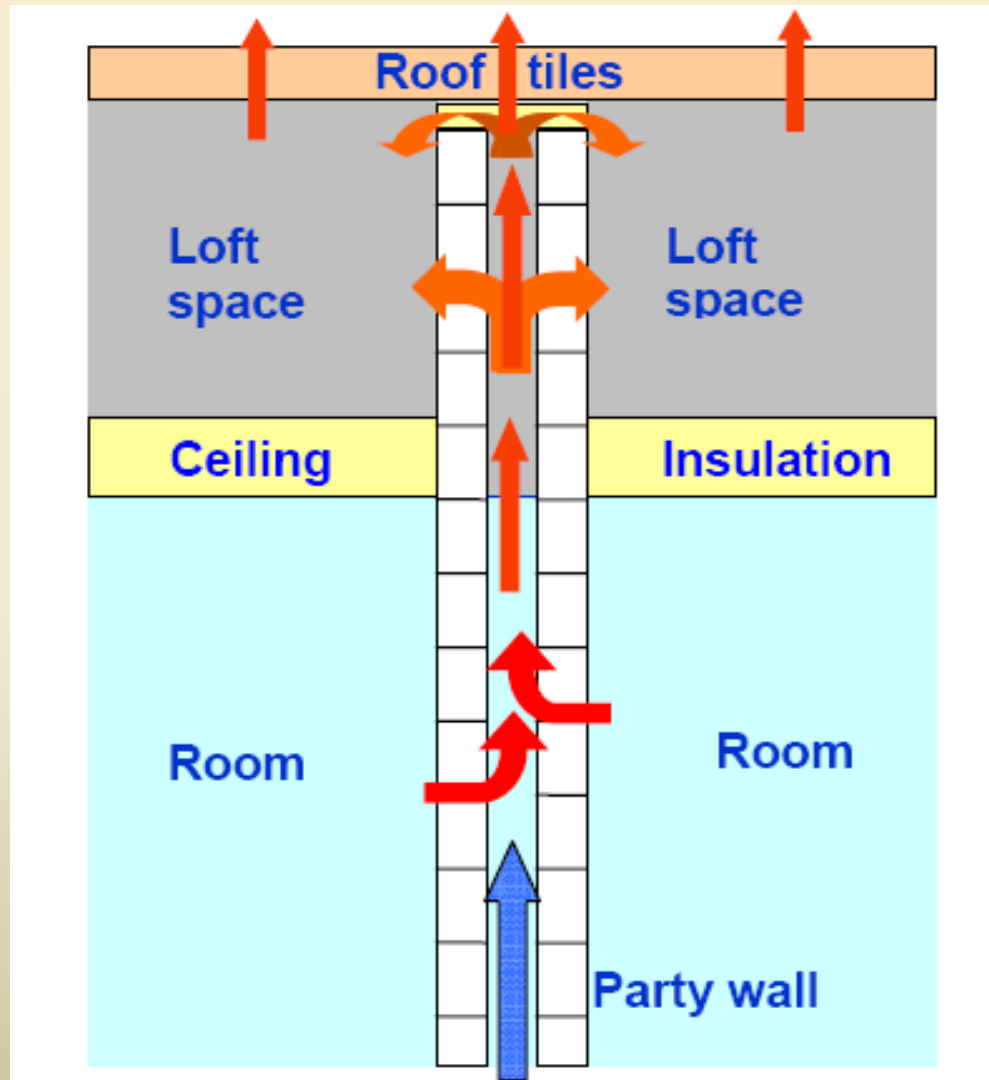
# Party wall bypass investigations – Stamford Brook



## Party wall bypass investigations – Stamford Brook



## Party wall bypass investigations – Stamford Brook





## Party wall bypass investigations – Stamford Brook



Party Wall

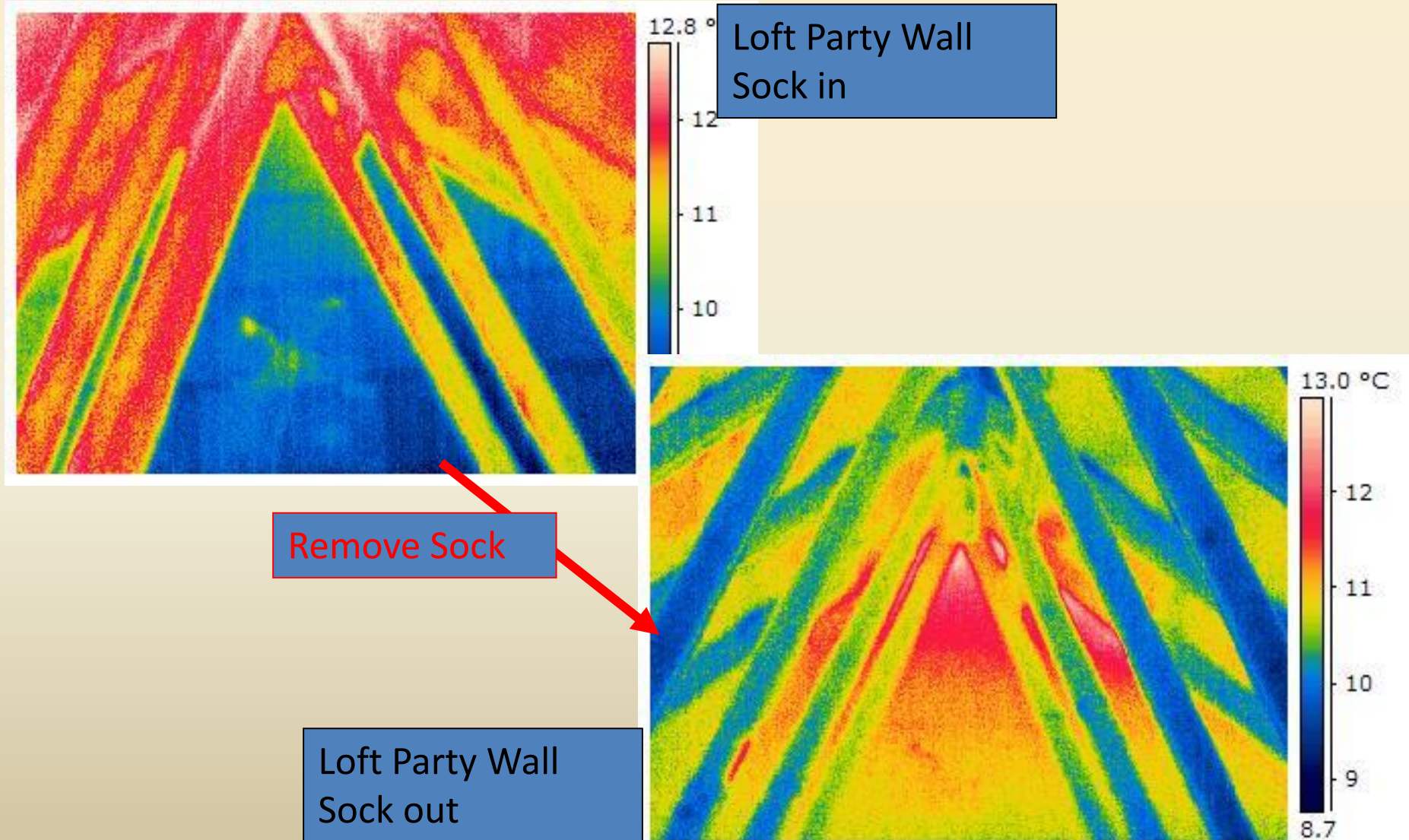


Cavity Sock



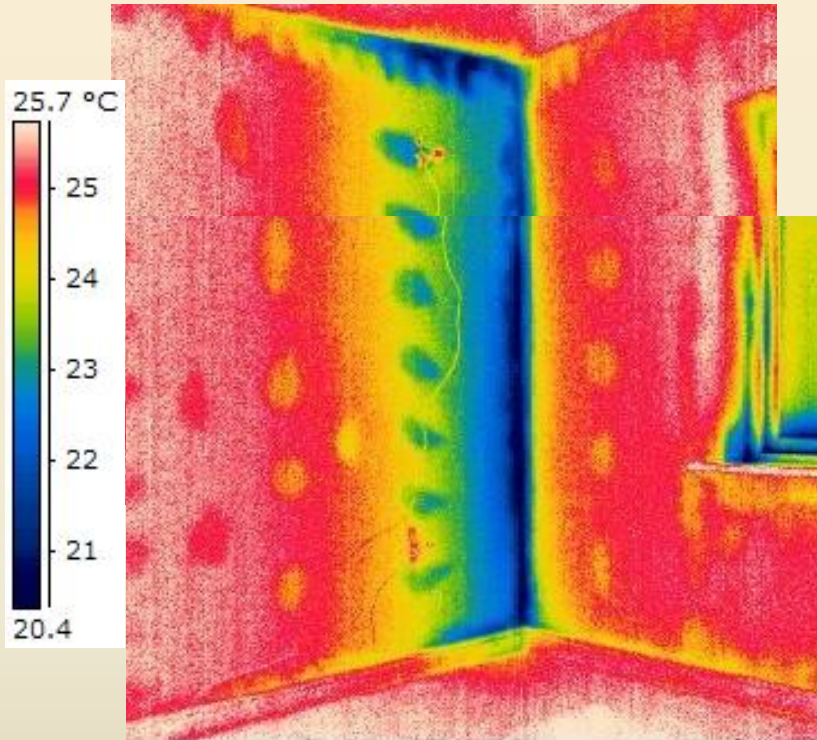
Removable Block

# Party wall bypass investigations – Stamford Brook





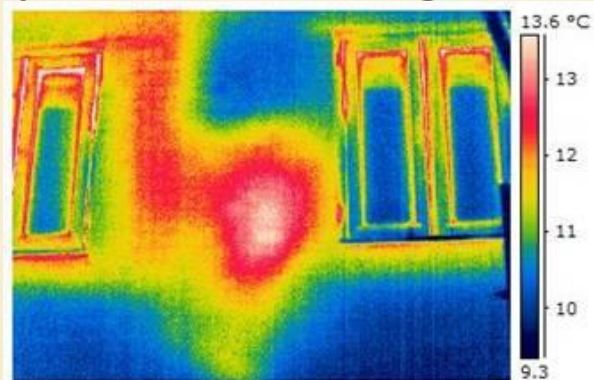
## Party wall bypass investigations – Stamford Brook



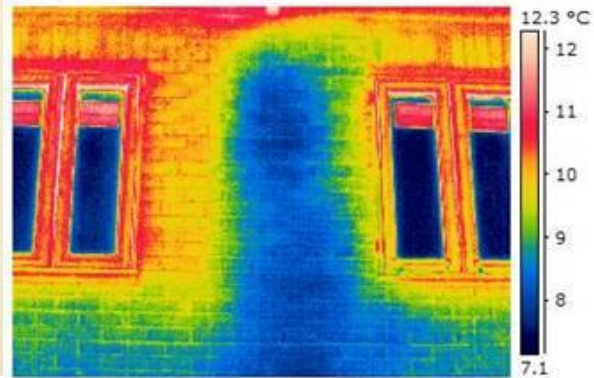
Second Floor – Party Wall to External  
Wall Junction – Sock Out

# Party wall bypass investigations – Stamford Brook

Party Wall  
Junction – Sock  
in Position



Party Wall  
Junction – Sock  
Removed



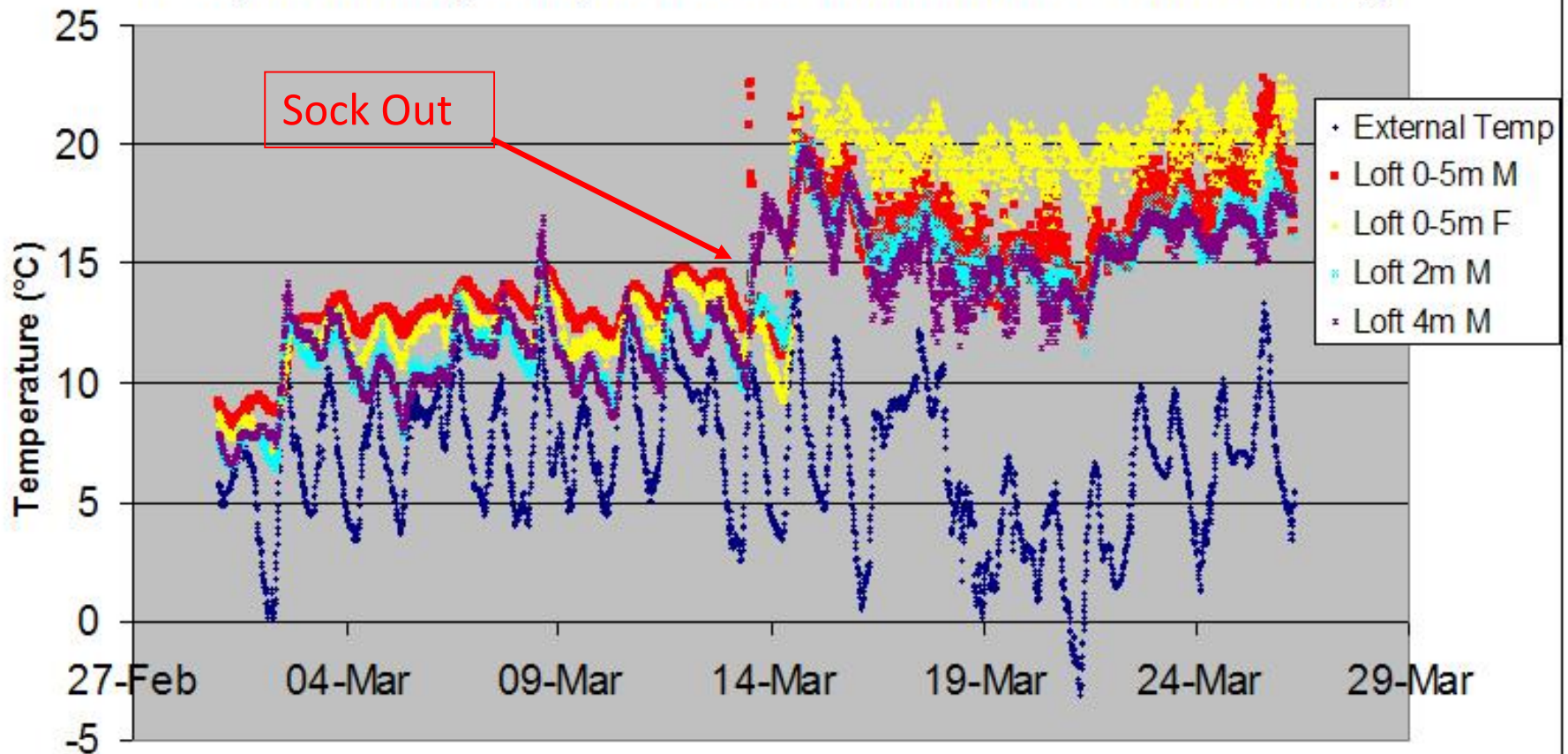
Party Wall  
Junction – Brick  
at Hot Spot  
Removed





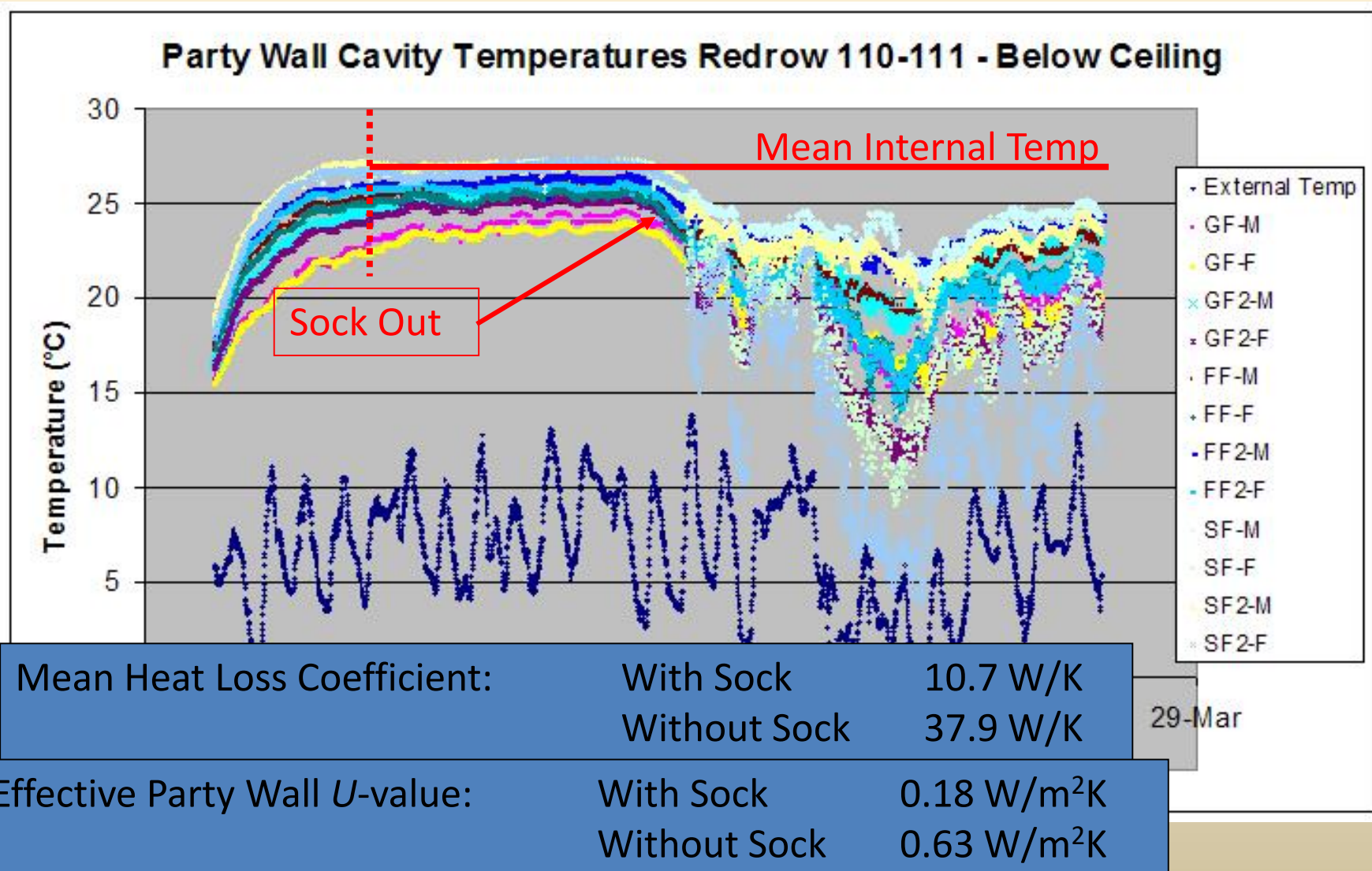
## Party wall bypass investigations – Stamford Brook

Party Wall Cavity Temperatures Redrow 110-111 - Above Ceiling



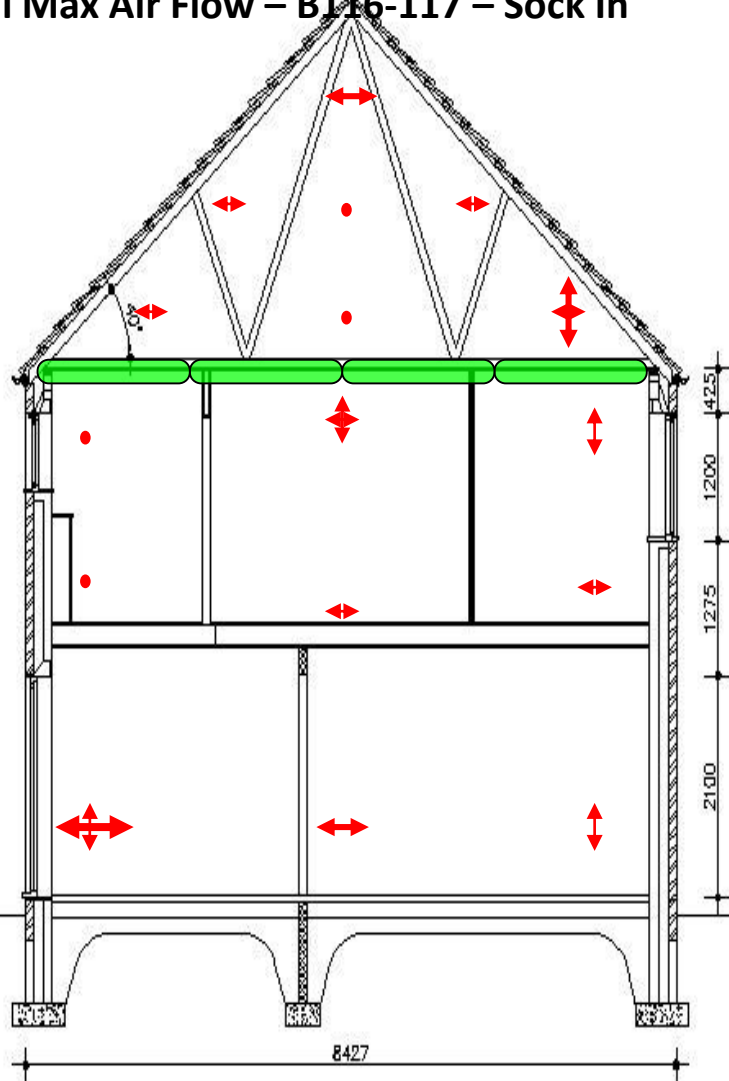


# Party wall bypass investigations – Stamford Brook

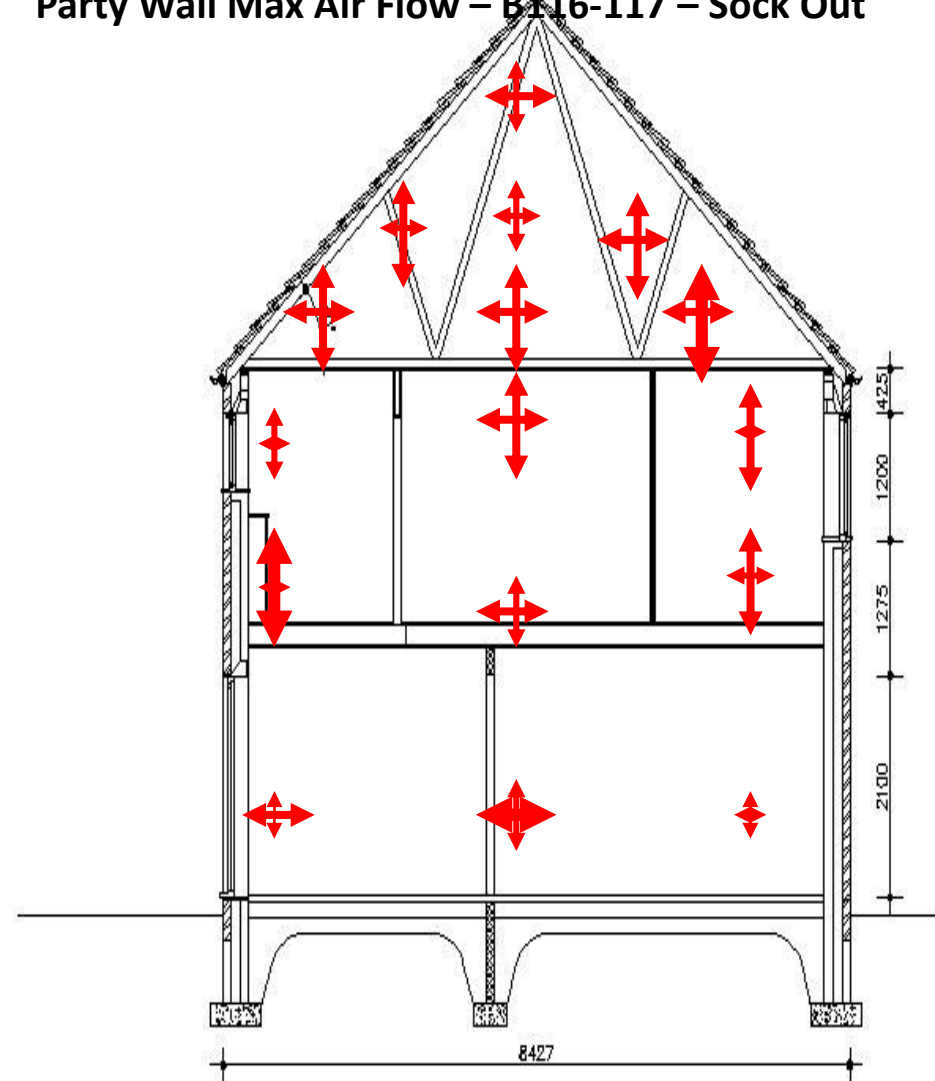


# Party wall bypass investigations – Stamford Brook

Party Wall Max Air Flow – B116-117 – Sock In



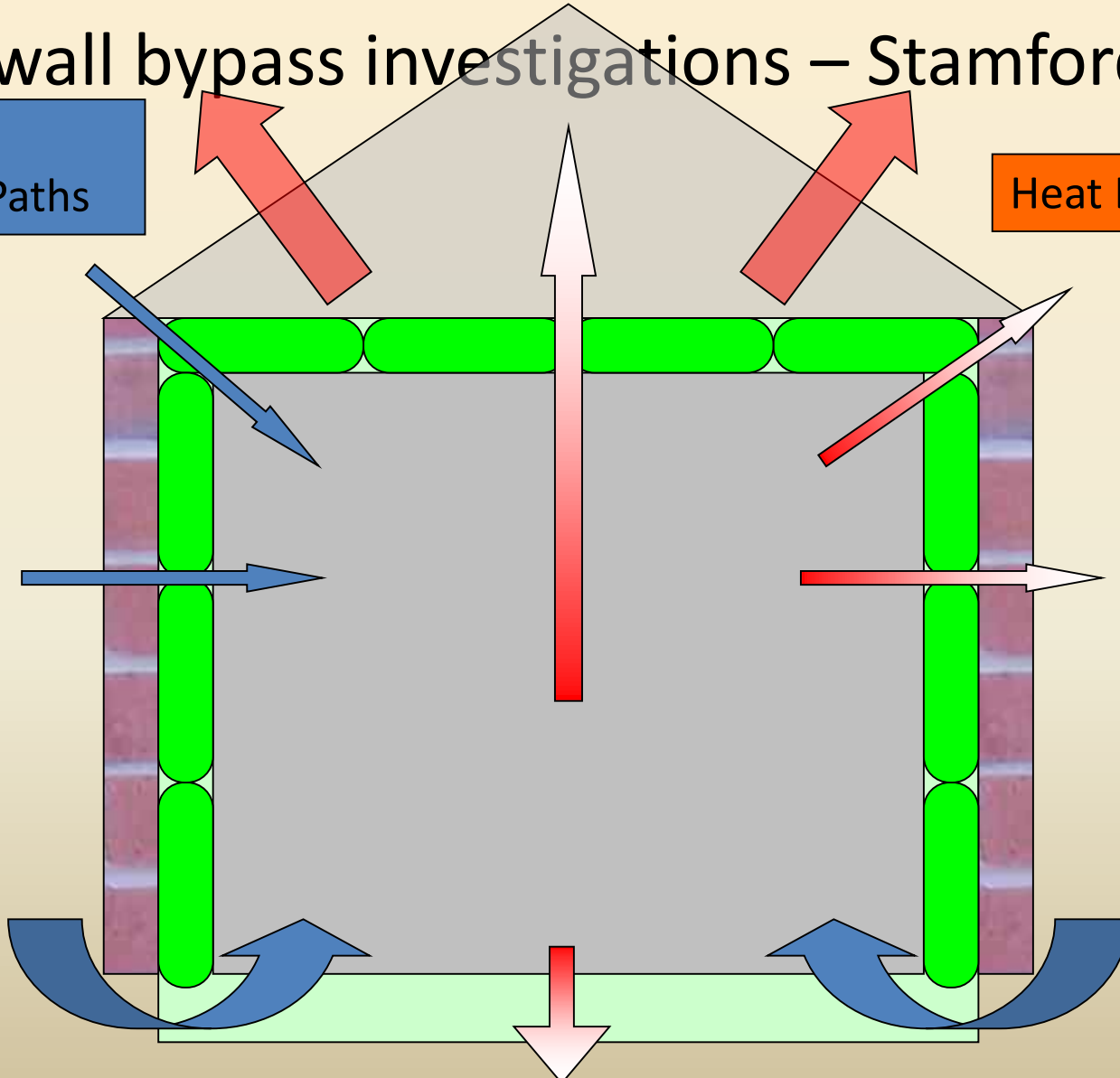
Party Wall Max Air Flow – B116-117 – Sock Out



## Party wall bypass investigations – Stamford Brook

Cold Air  
Infiltration Paths

Heat Loss Paths



## Party wall bypass investigations – Stamford Brook

### Party Wall Bypass – Estimated UK CO<sub>2</sub> savings if bypass eliminated

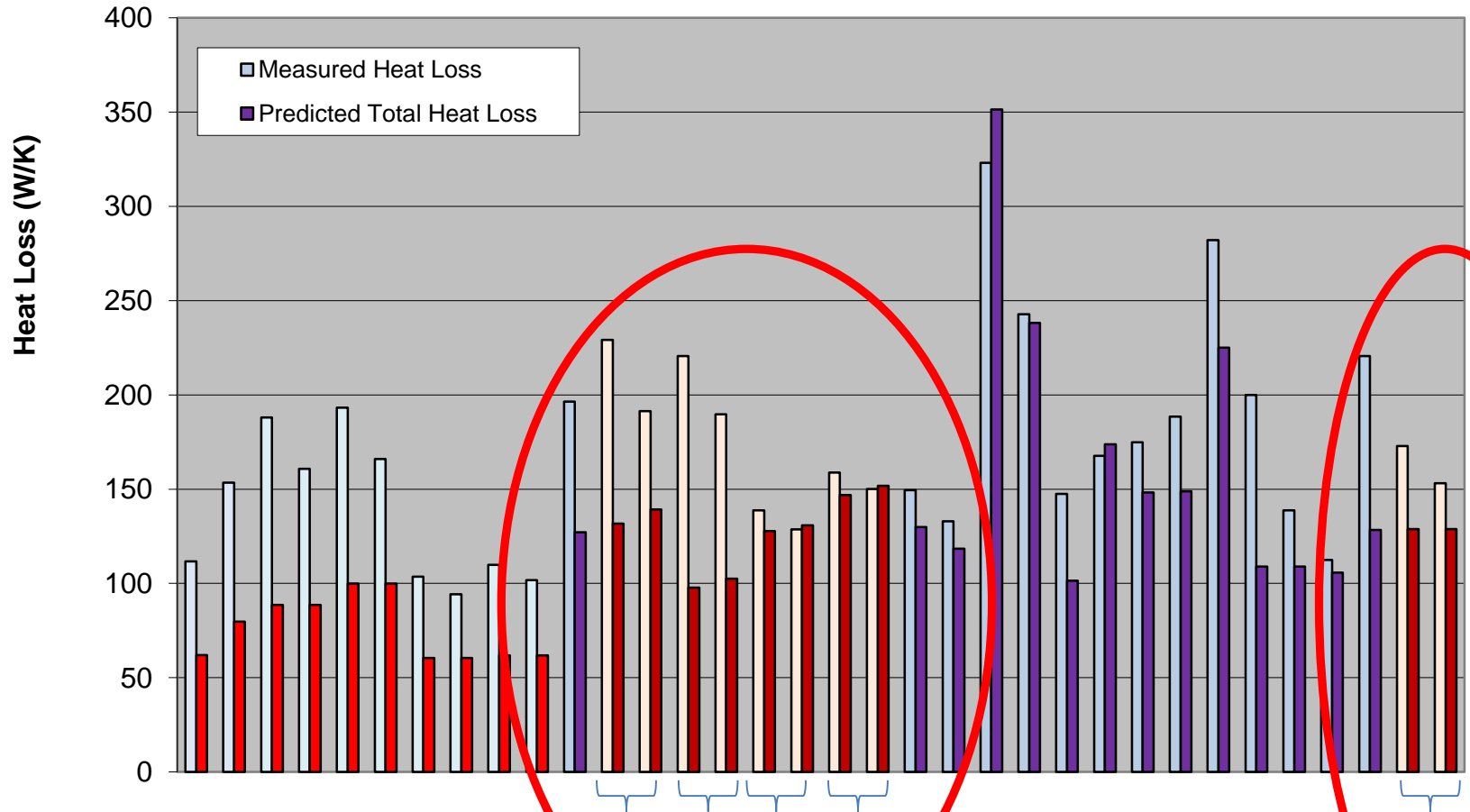
|   |                              |
|---|------------------------------|
| From New Housing<br>built in One Year<br>(~190,000 units) | 18,000 tCO <sub>2</sub> /a   |
| From Existing Stock<br>(built since 1965)                 | ~750,000 tCO <sub>2</sub> /a |

Assumes Party Wall  $U$ -Value = 0.5 W/m<sup>2</sup>K

Assumes 10% semi-detached, 20% terrace in stock and new build

Calculations for semis and terraces only – no estimate for apartments

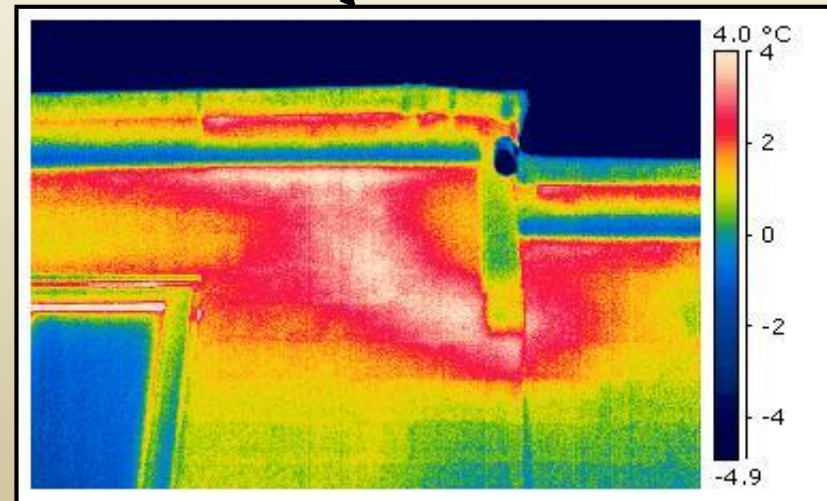
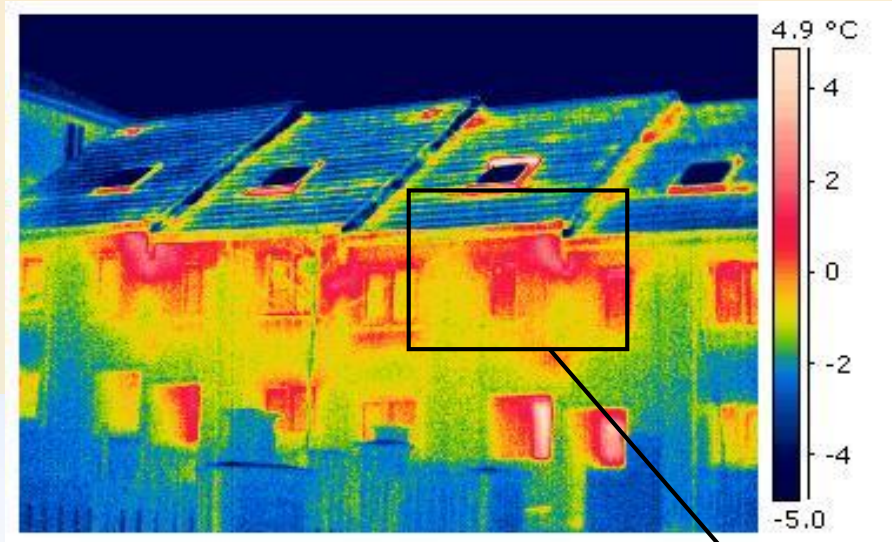
## Whole House Heat Loss - Measured Coheating versus Predicted



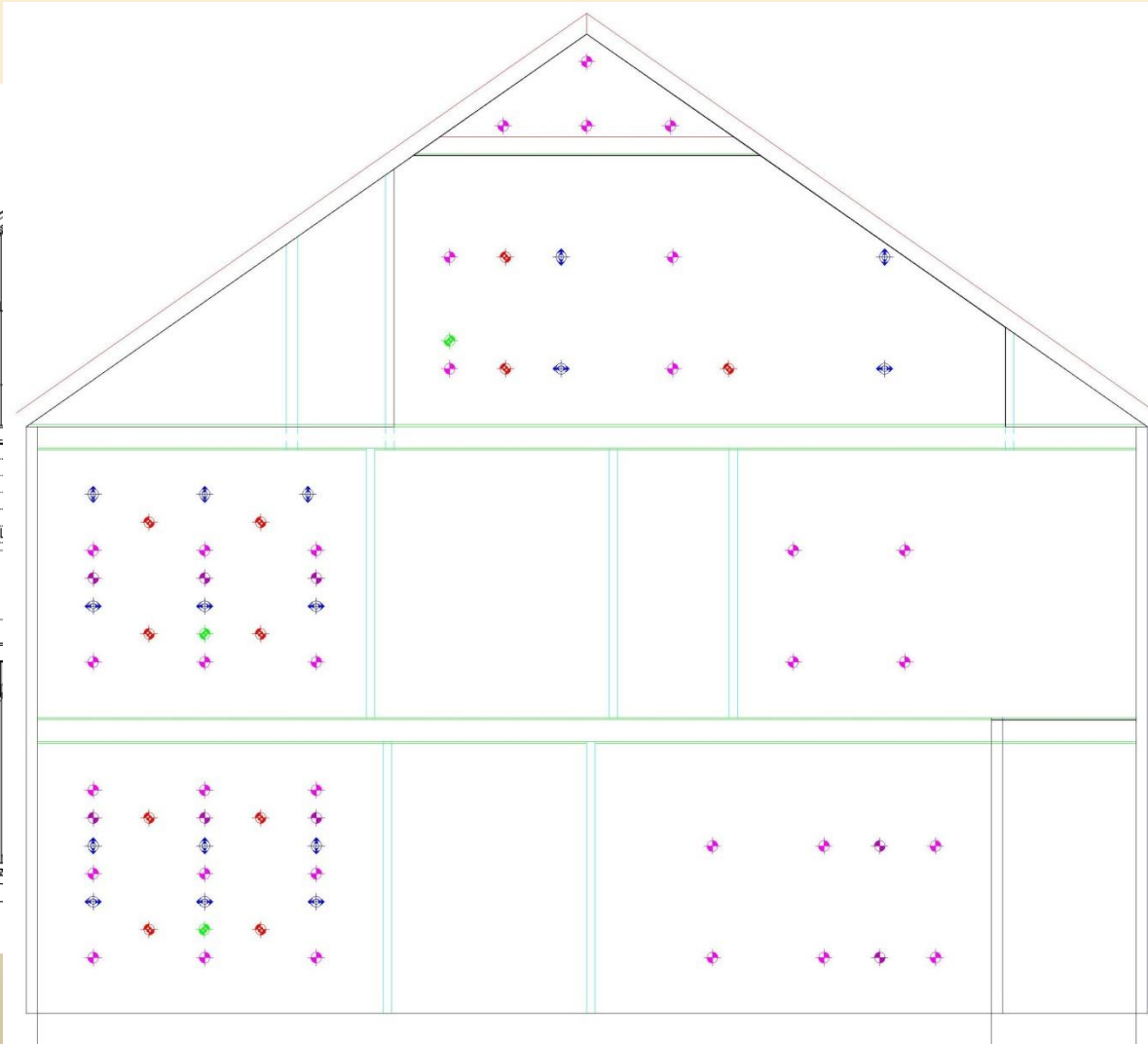
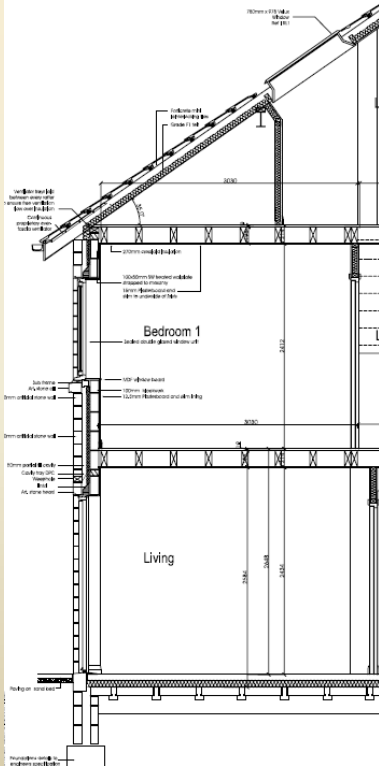
Party wall bypass investigations – EURISOL / MIMA



# Party wall bypass investigations – EURISOL / MIMA



# Party wall bypass investigations – EURISOL / MIMA



◆ Party wall cavity temperature

◆ Party wall surface temperature

◆ Internal/cavity differential pressure

◆ Heat flux

◆ Party wall cavity airflow - horizontal

◆ Party wall cavity airflow - vertical

# Party wall bypass investigations – EURISOL / MIMA

Surface Thermocouple

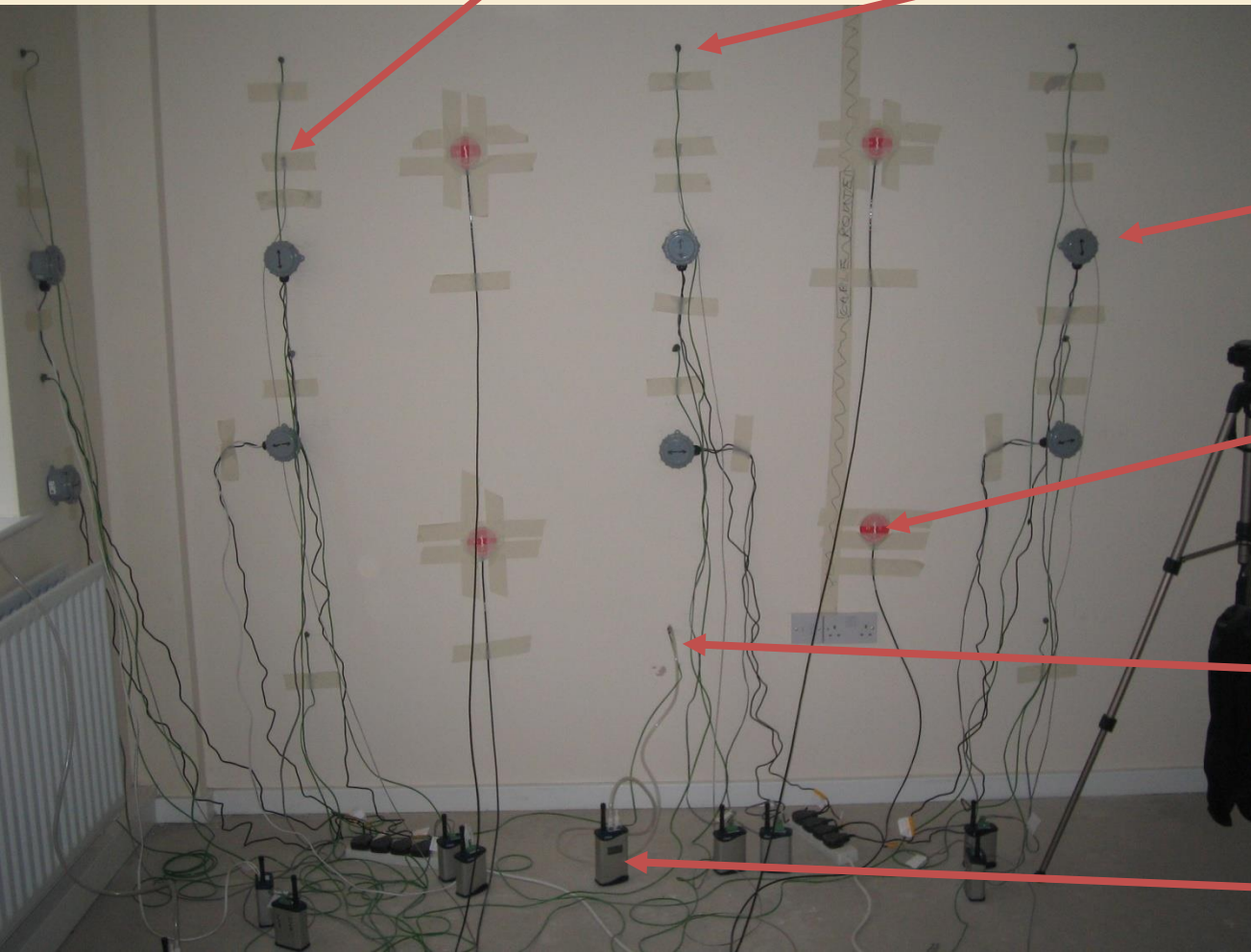
Cavity Thermocouple

Air Flow  
Transducer

Heat Flux Plate

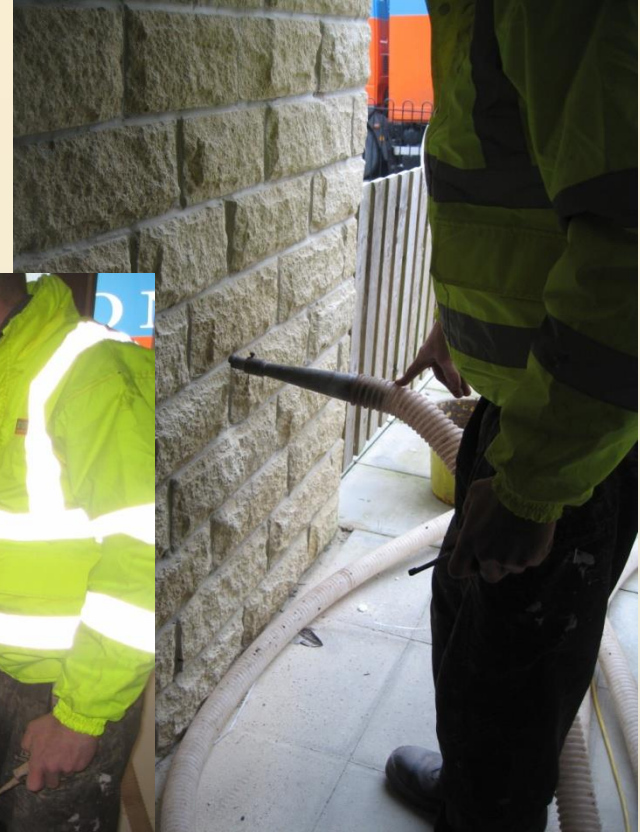
Differential  
Pressure

Transmitter



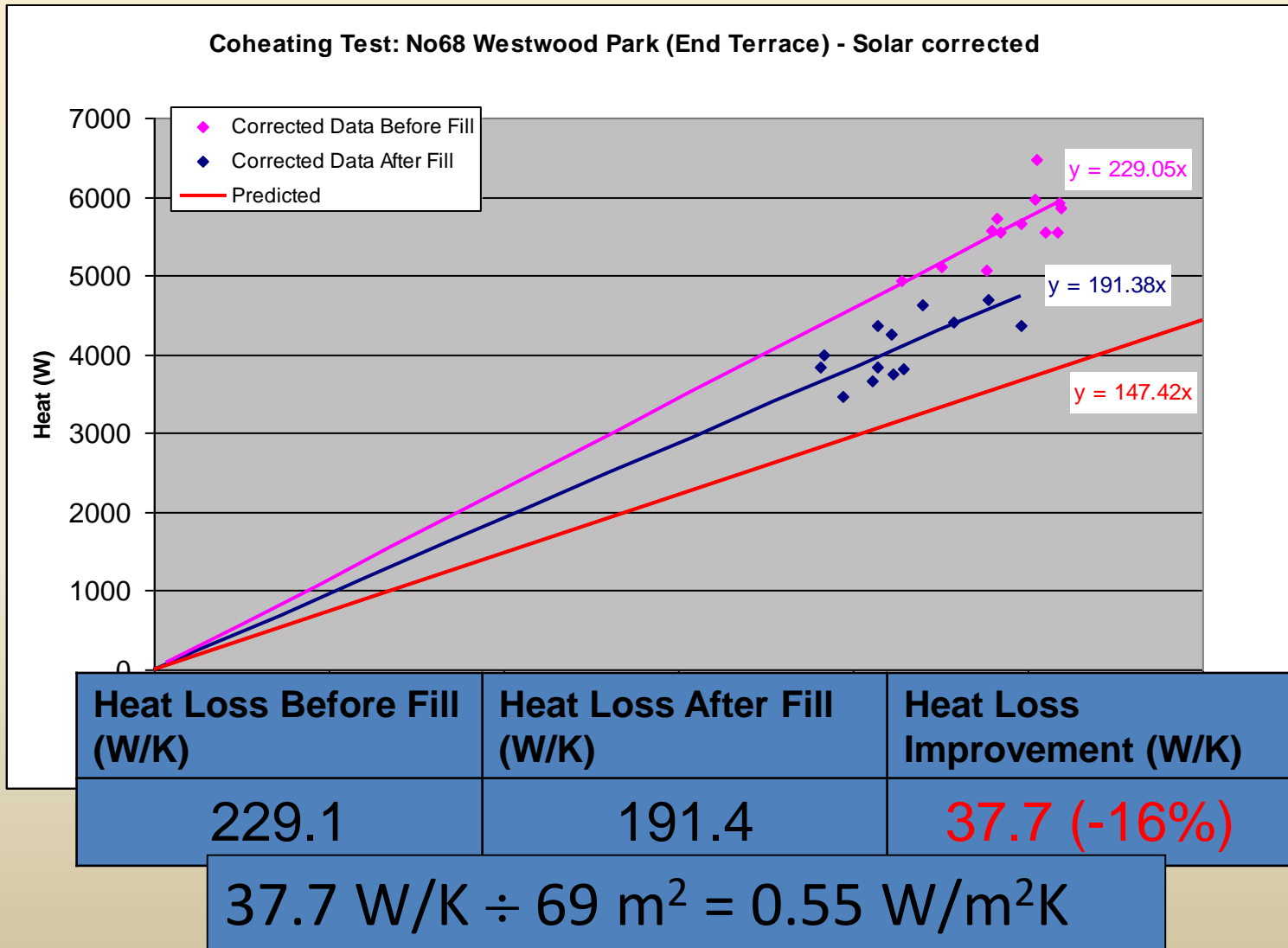


## Party wall bypass investigations – EURISOL / MIMA

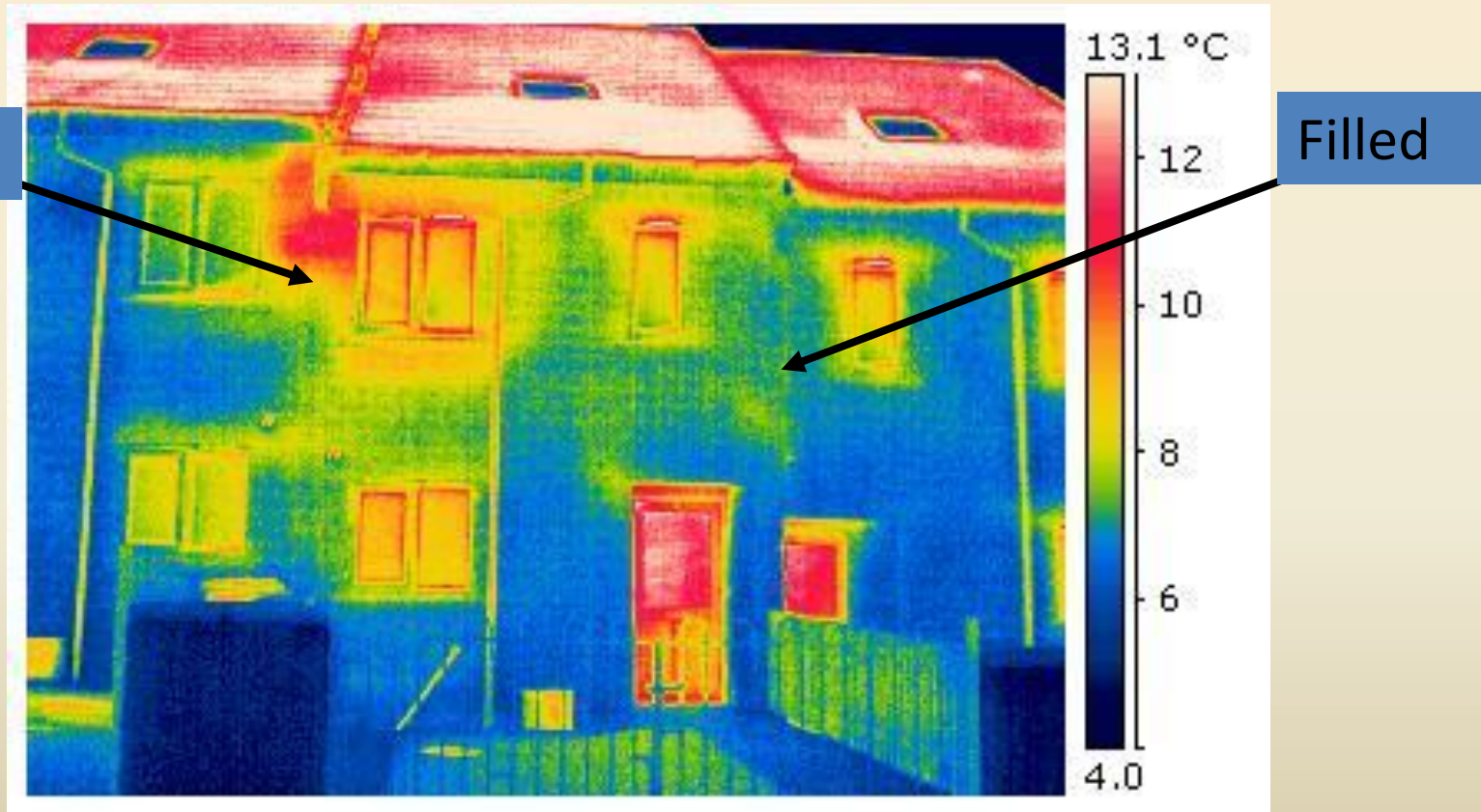


- Material: Knauf Supafil Plus 40
- Usage: ~6 bags = 106kg over ~72.4m<sup>2</sup> (Cavity ~75mm)
- Estimated fill density: ~19.6 kg/m<sup>3</sup> (Volume ~ 5.4m<sup>3</sup>)

# Party wall bypass investigations – EURISOL / MIMA

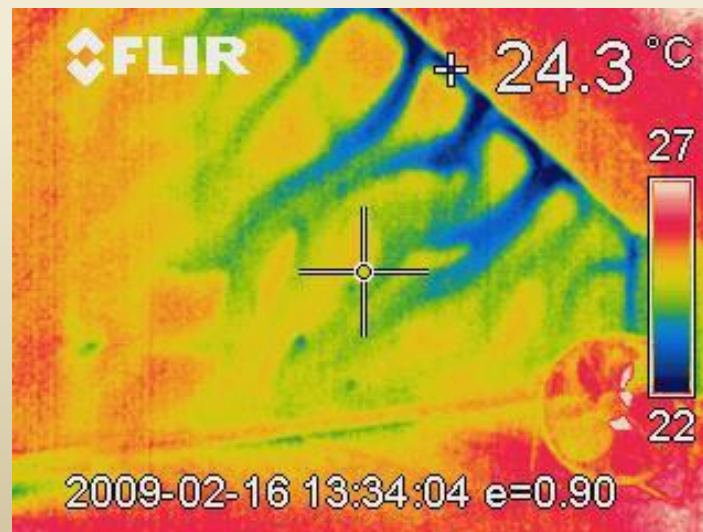
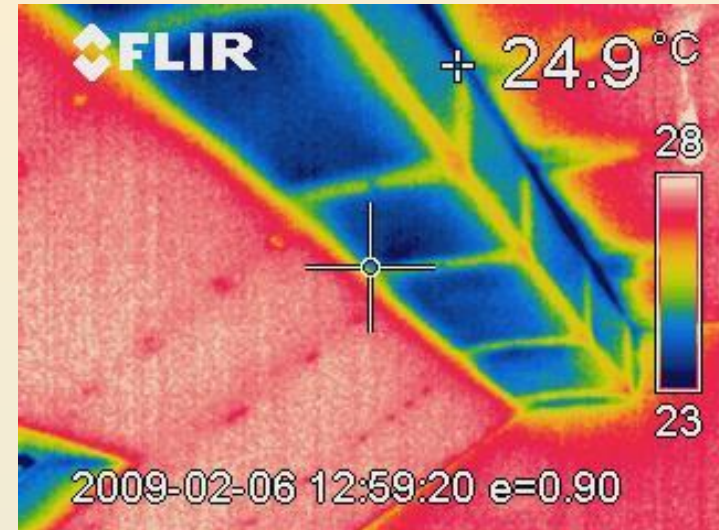
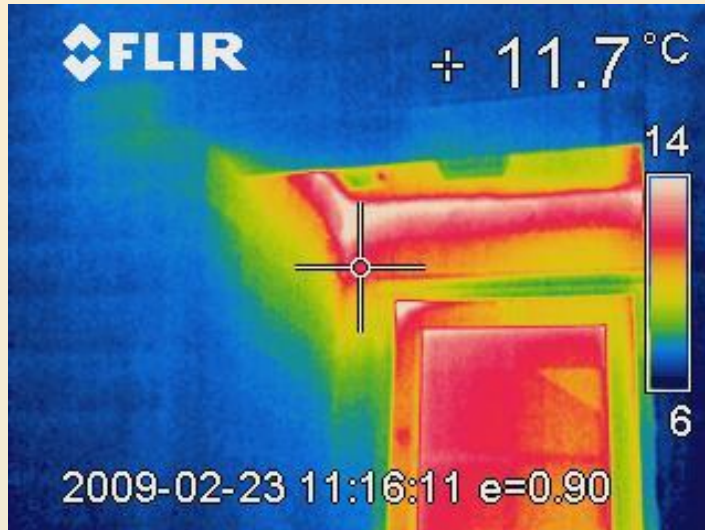


## Party wall bypass investigations – EURISOL / MIMA





## Party wall bypass investigations – EURISOL / MIMA



# Implications for Building Regulations



L1A

## Section 5: Quality of construction and commissioning

CRITERION 4 – BUILDING PERFORMANCE CONSISTENT WITH DER

Fully filling the cavity may have implications for sound transmission through party walls. Developers who follow this route must satisfy the BCB that the requirements of Part E will be satisfied, either by adopting a full fill detail accredited under

## L1A QUALITY OF CONSTRUCTION AND COMMISSIONING

Table 3 U-values for party walls

| Party wall construction   | U-value (W/m <sup>2</sup> K) |
|---|------------------------------|
| Solid   | 0.0                          |
| Unfilled cavity with no effective edge sealing  | 0.5                          |
| Unfilled cavity with effective sealing around all exposed edges and in line with insulation layers in abutting elements   | 0.2                          |
| A fully filled cavity with effective sealing at all exposed edges and in line with insulation layers in abutting elements | 0.0                          |

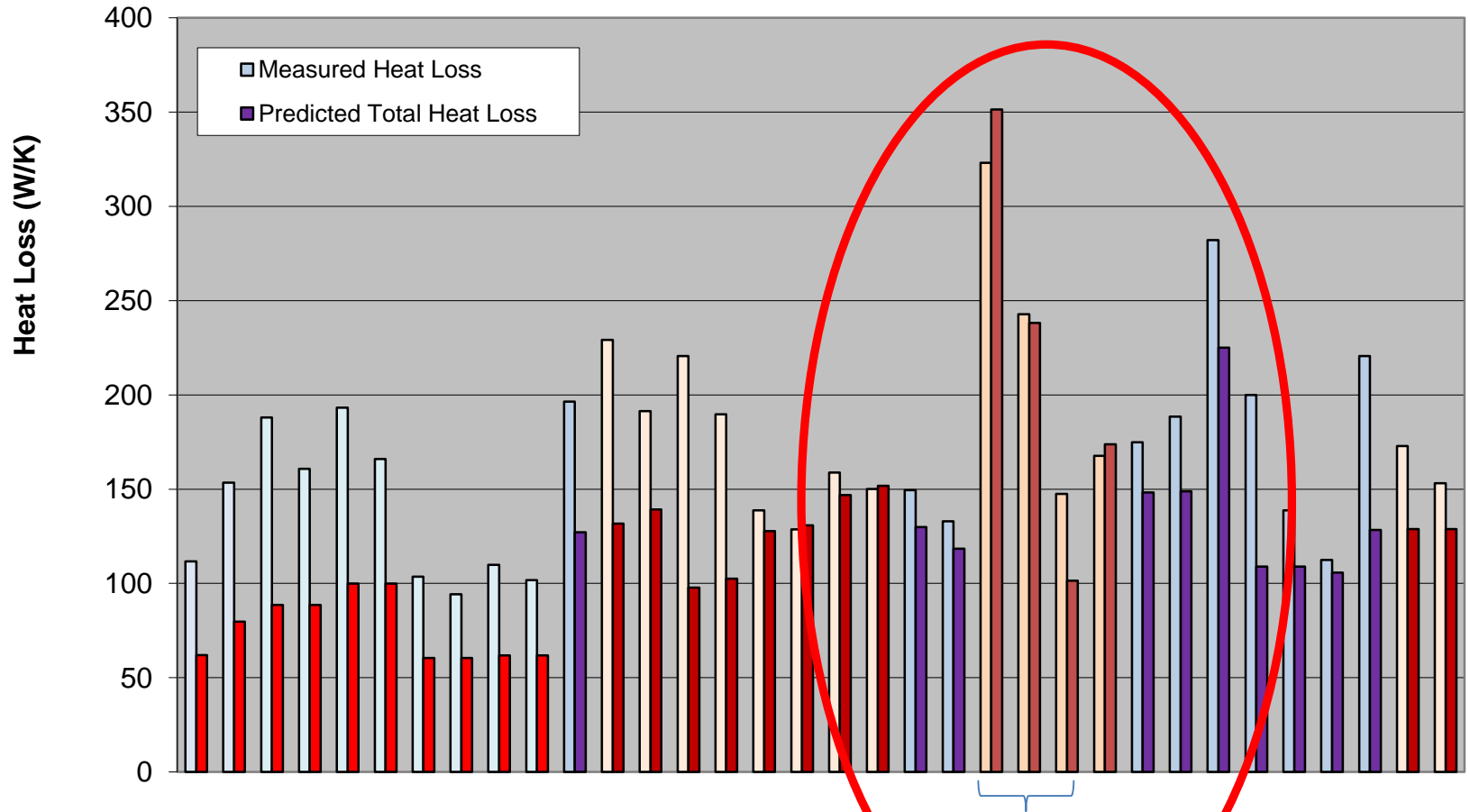
**5.8** The party wall is a particular case of the more general thermal bypass problem that occurs where the air barrier and the insulation layer are not contiguous and the cavity between them is subject to air movement. To avoid the consequent reduction in thermal performance, either the insulation layer should be contiguous with the air barrier at all points in the building envelope, or the space between them should be filled with solid material such as in a masonry wall.

### Thermal bridges

*For new buildings, such scheme(s) accredit and quality assure the calculation of the linear thermal transmittance, accredit details in terms of buildability and have an associated quality assurance regime that inspects a sample of sites to confirm that the details are being implemented correctly. The use of such schemes may also allow a reduction in the Building Control charges.*

- To use details that have not been subject to independent assessment of the construction method. However, in this case, the linear thermal transmittance should still have been

## Whole House Heat Loss - Measured Coheating versus Predicted



Existing dwellings

## 2009/10: Temple Avenue Project, York



Project funded by the  
Joseph Rowntree Housing  
Trust



Thin-Joint Masonry & SIPs Construction  
Code for Sustainable Homes Level 4  
Prototypes for a 540-home development

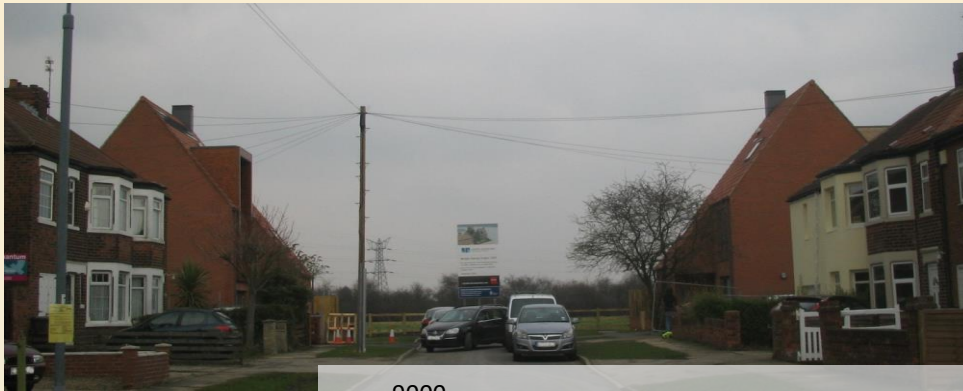


Standard 1930's semi-detached property  
2-stage refurbishment:

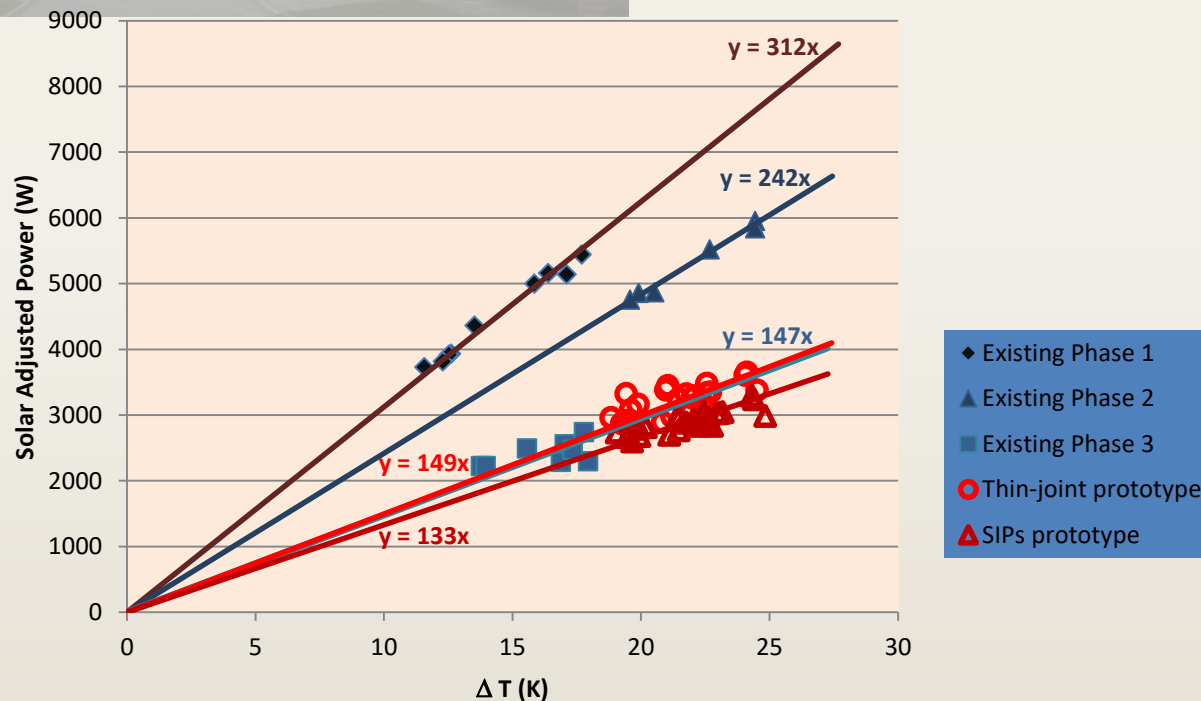
1. Standard decent homes upgrade
2. Enhance energy performance to the same level as the prototypes



# 2009/10: Temple Avenue Project, York

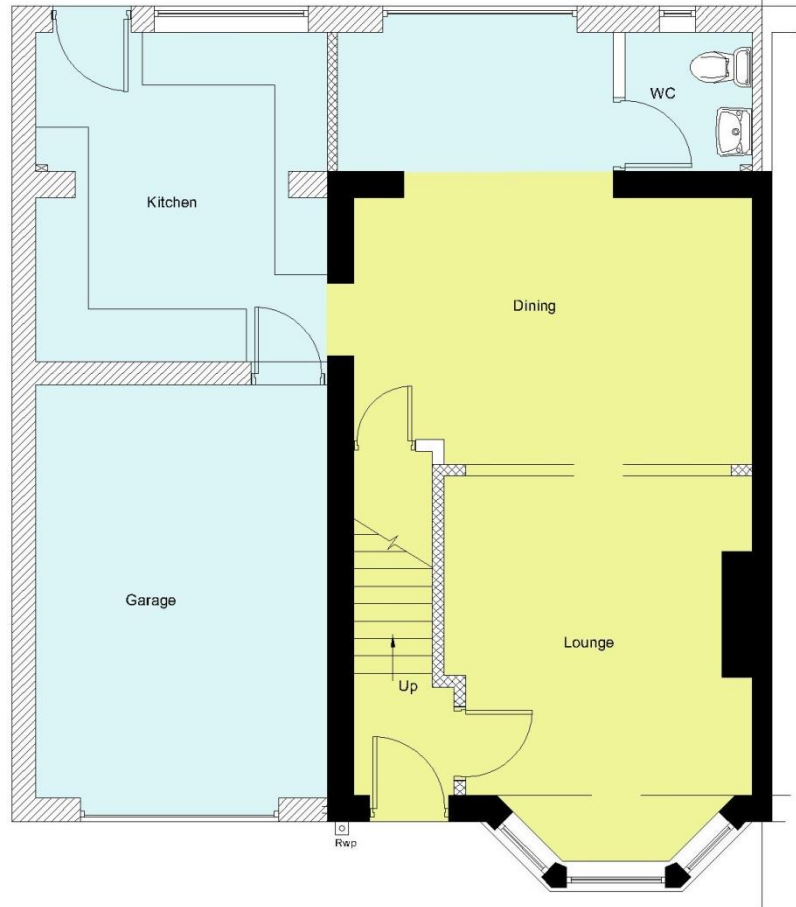


Project funded by the Joseph Rowntree Housing Trust

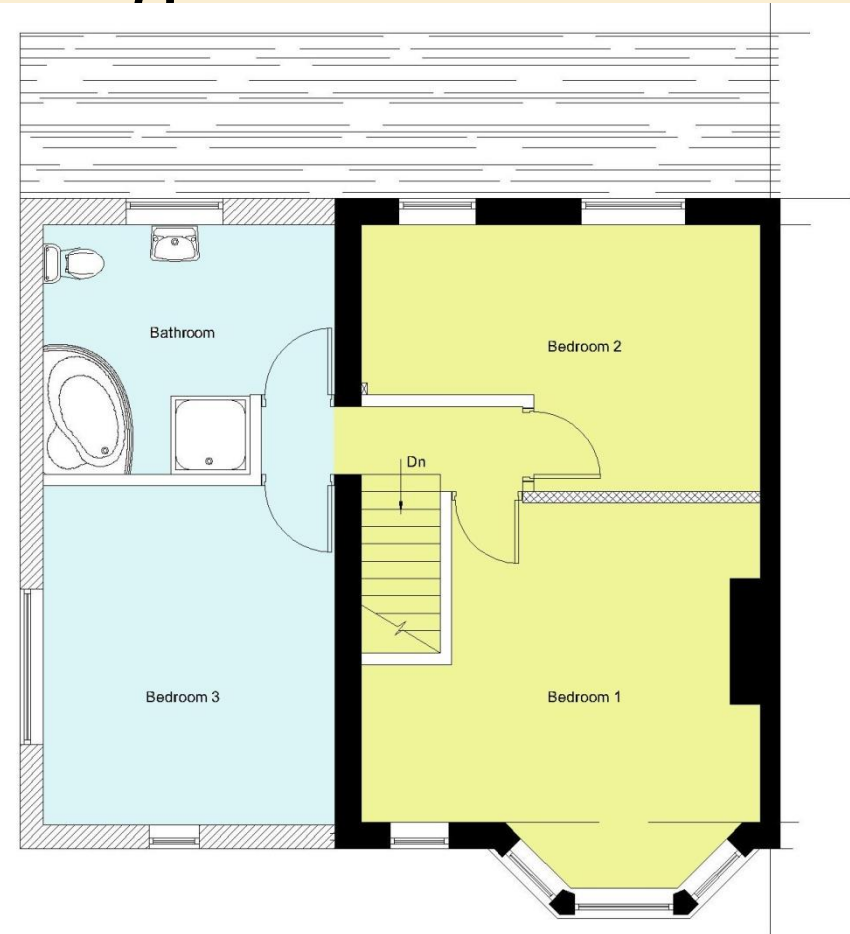




## Existing dwelling - TAP

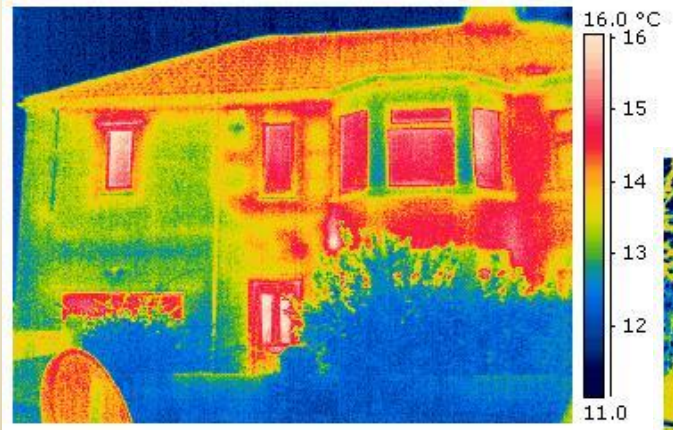


GROUND FLOOR PLAN

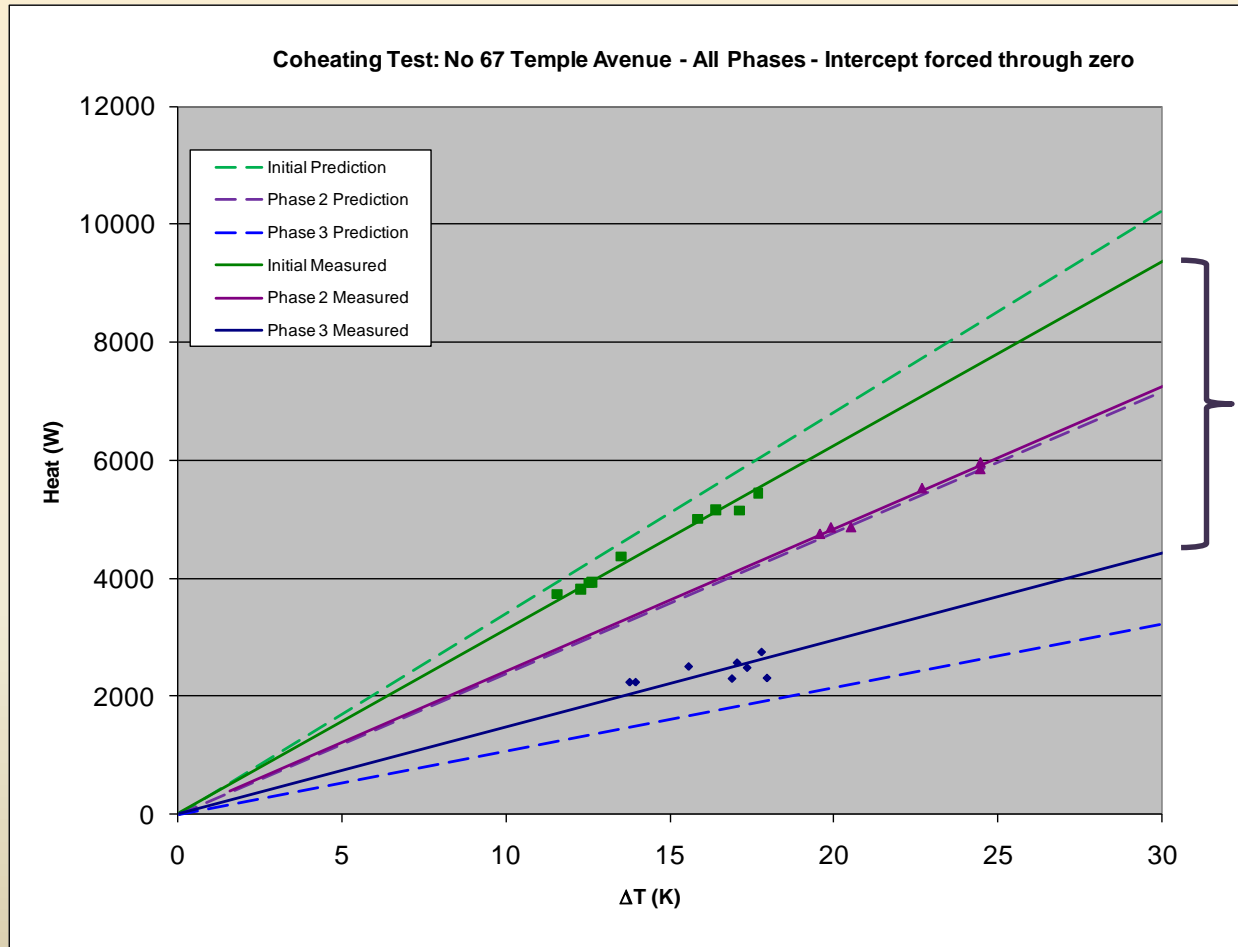


FIRST FLOOR PLAN

## Existing dwellings - TAP



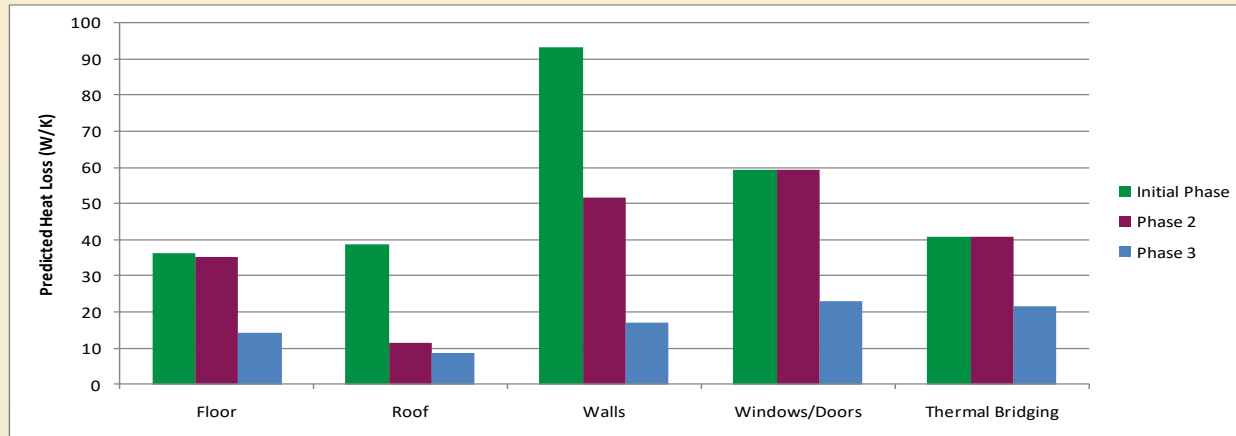
# Existing dwelling - TAP



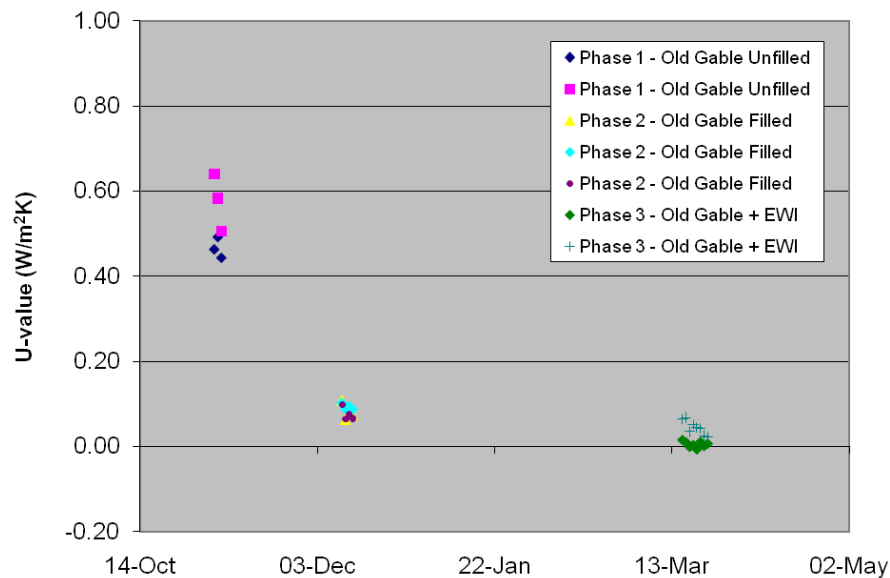
Actual Reduction

Theoretical Reduction

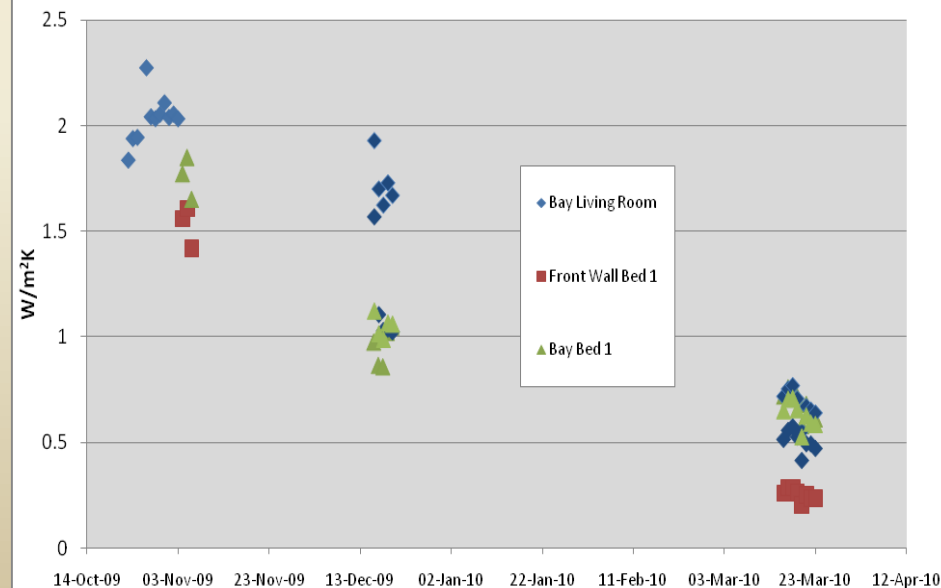
# Existing dwellings - TAP



67 Temple Avenue Old Gable Wall - Before and After CWI & EWI

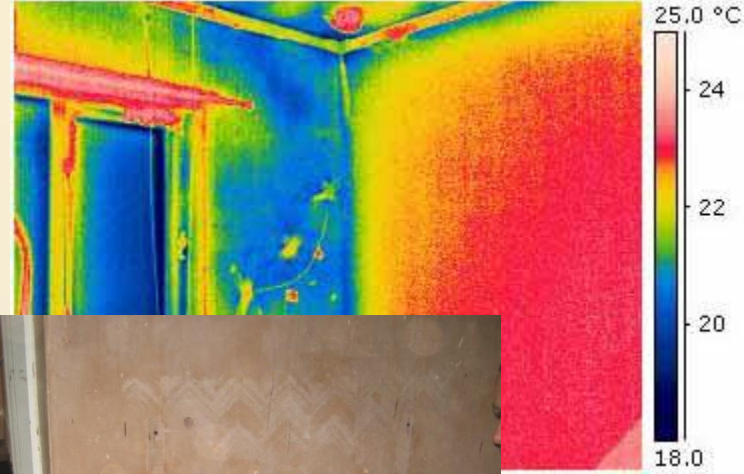
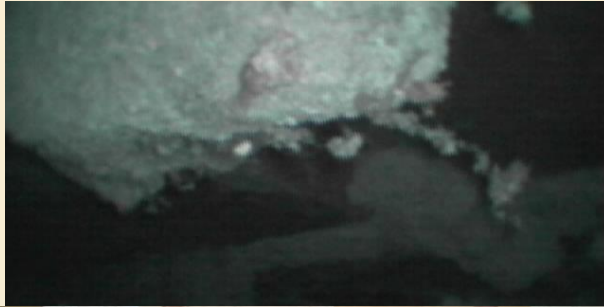


67 Temple Avenue - Measured wall U-values pre- and post-CWI & EWI

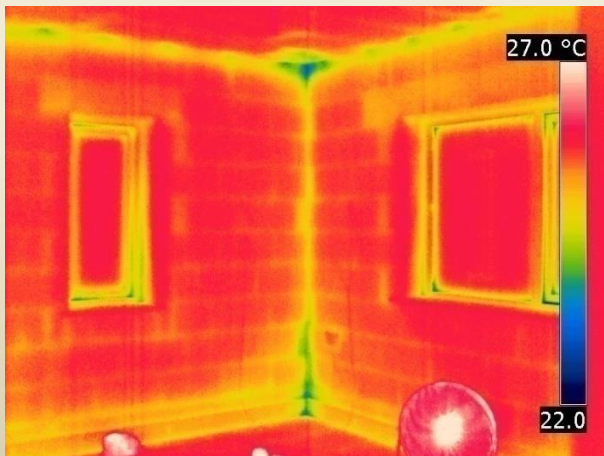




## Existing dwellings - TAP



## Existing dwellings - TAP

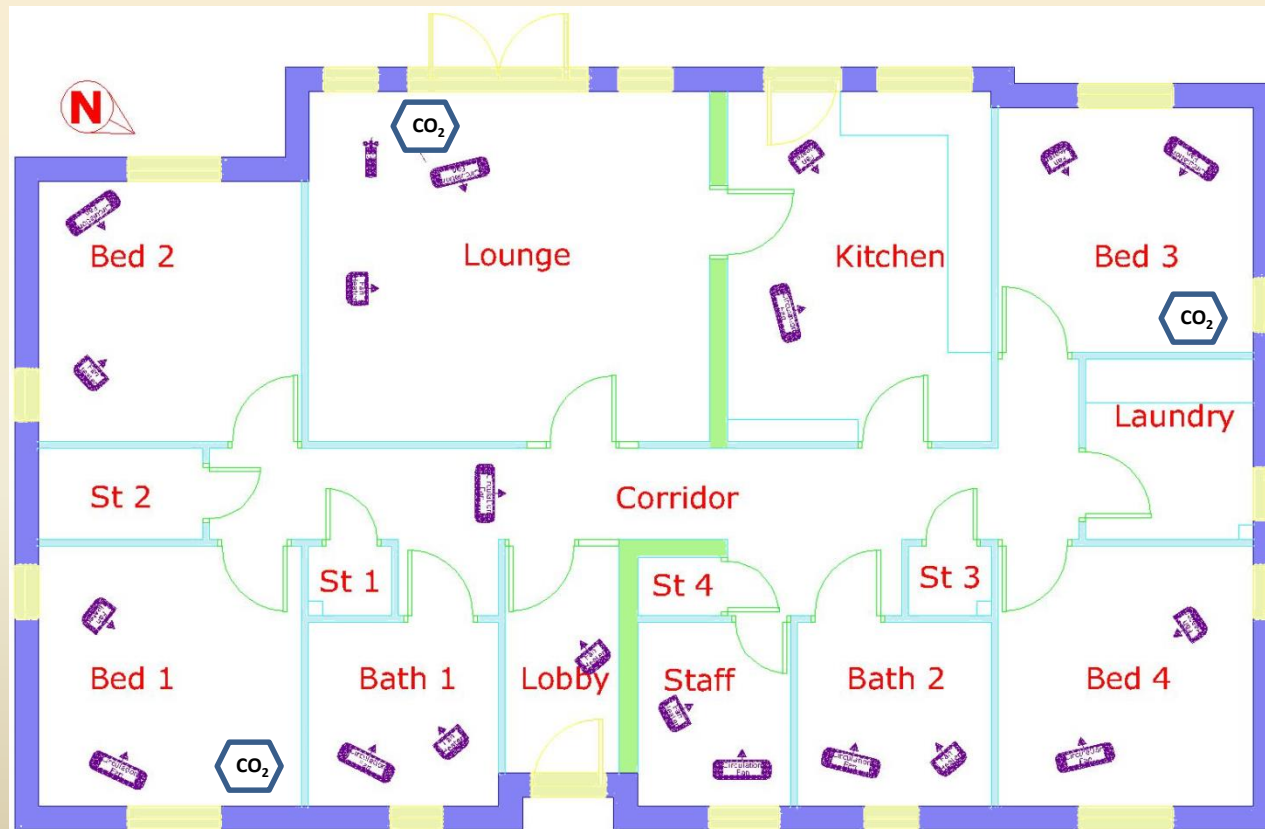




## Existing dwellings - TAP



# Closing the Loop





# Closing the Loop

## Ventilation Heat Loss

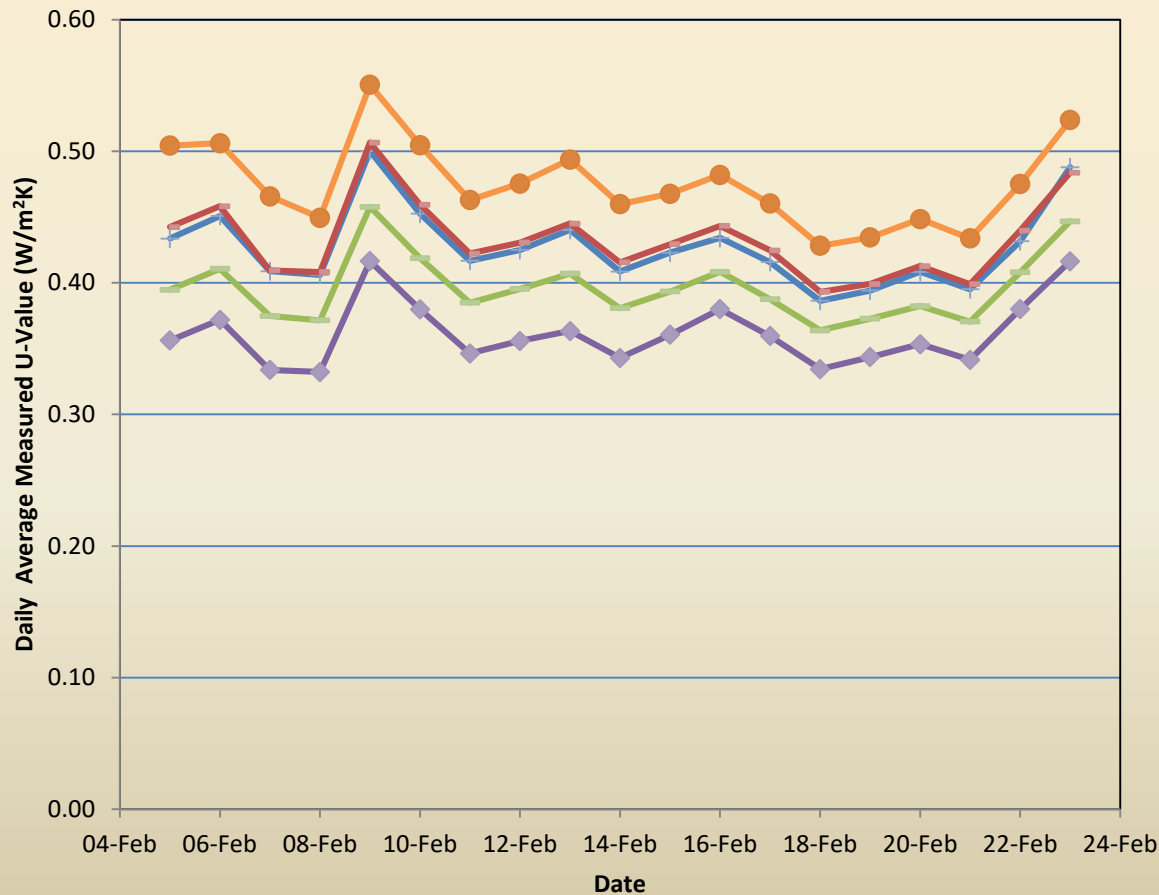
| Air Permeability ( $\text{m}^3/(\text{h} \cdot \text{m}^2)$ @ 50Pa) |                |                          |               |                | Mean Permeability used for coheating calculations |
|---|----------------|--------------------------|---------------|----------------|---|
| Date  | 09-Nov-10      | 14-Jan-11                | 01-Feb-11     | 25-Feb-11      |   |
| Plot 6  | 9.28           | 3.85                     | 4.31          | 4.48           | 4.395   |
|   | pre-completion | Building Regs compliance | pre-coheating | post-coheating | (5.15 $\text{h}^{-1}$ @50Pa)                      |

| Ventilation Rate ( $\text{h}^{-1}$ , (Roulet & Foradini 2002)) |             |             |             | Mean Wind Speed |
|--|-------------|-------------|-------------|-----------------|
| Date   | Bedroom 1   | Lounge      | Bedroom 3   |                 |
| 11 Feb   | <b>0.31</b> | <b>0.32</b> | <b>0.31</b> | <b>1.02</b>     |
| 12 Feb   | <b>0.29</b> | <b>0.31</b> | <b>0.30</b> | <b>1.75</b>     |
| 13 Feb   | <b>0.35</b> | <b>0.38</b> | <b>0.35</b> | <b>2.64</b>     |
| 19 Feb   | <b>0.35</b> | <b>0.34</b> | <b>0.34</b> | <b>1.74</b>     |
| 20 Feb   | <b>0.35</b> | <b>0.37</b> | <b>0.34</b> | <b>2.04</b>     |



# Closing the Loop

## External Wall Measurements



- K 1 - External wall 1
- K 2 - External wall 2
- K 3 - External wall 3
- K 4 - External wall 4
- K 5 - External wall 5



# Closing the Loop

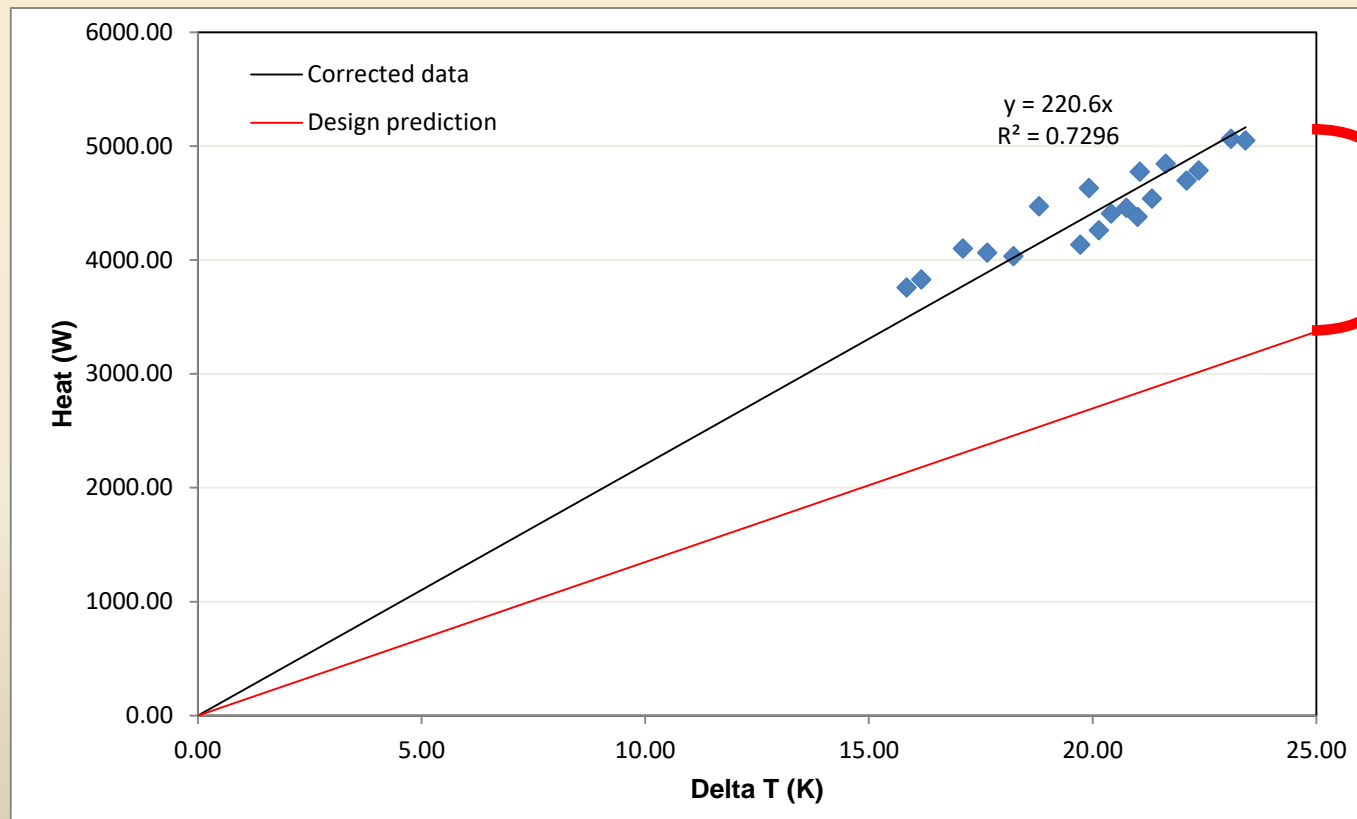
## External Wall Measurements



4 5  
3  
1 2



# Closing the Loop

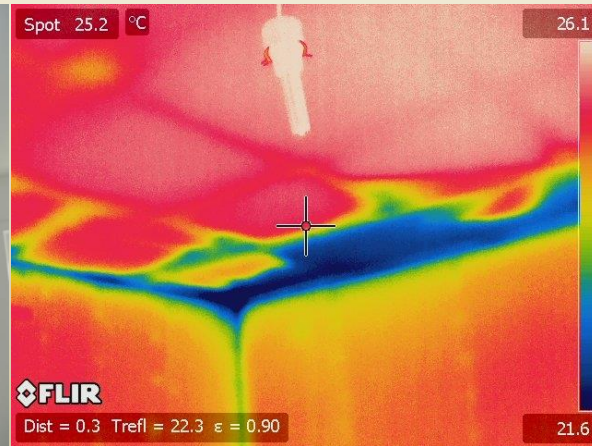
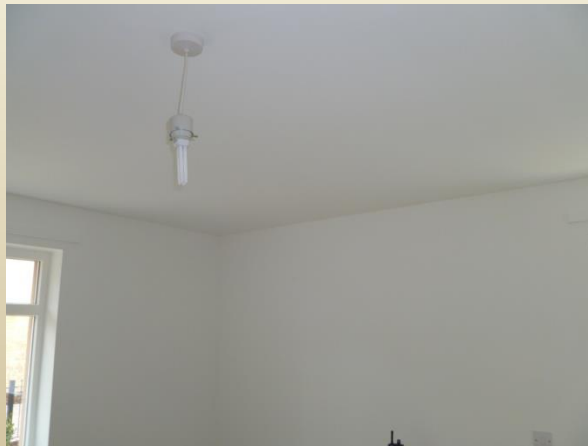


**64% greater  
heat loss than  
predicted**



# Closing the Loop

## Thermal Bridging

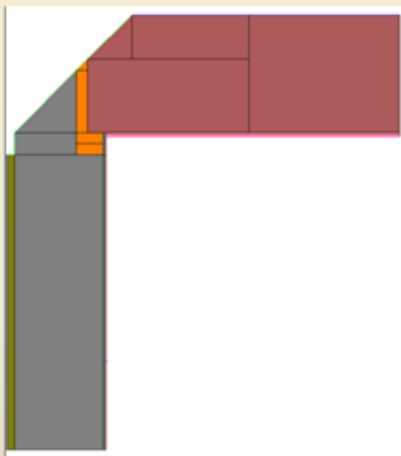




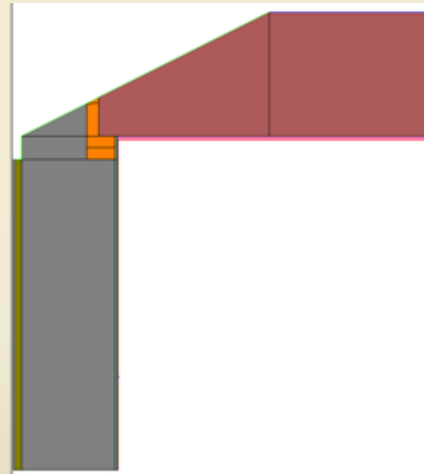
# Closing the Loop

## Thermal Bridging

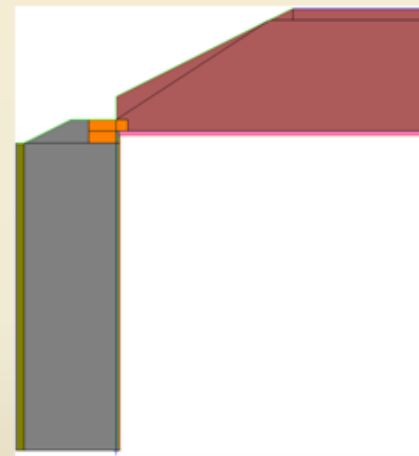
Therm 5.2 model: 300mm Hemcrete ( $\lambda = 0.06$  W/mK), 89mm Timber stud ( $\lambda = 0.13$  W/mK), 400mm Loft insulation ( $\lambda = 0.042$  W/mK)



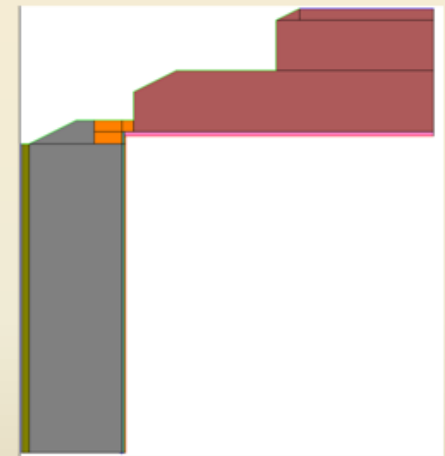
$\Psi = 0.026$  W/mK  
45° Pitch



$\Psi = 0.043$  W/mK  
30° Pitch



$\Psi = 0.084$  W/mK  
'as-built' - ideal



$\Psi = 0.109$  W/mK  
'as-built' - practice

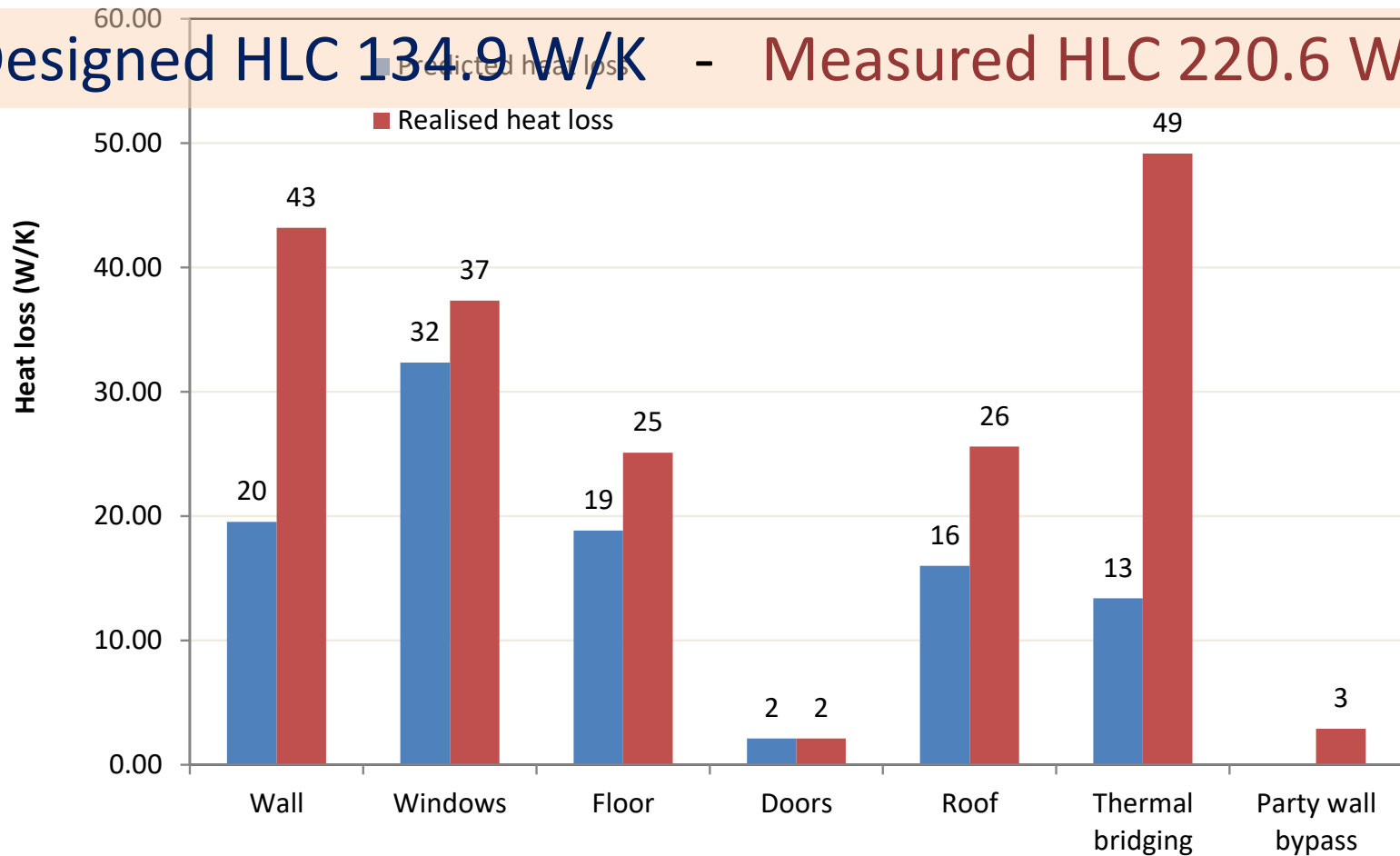
SAP 2009, Appendix Q, Table K1 :

Eaves detail to ACD  
Default value

$\Psi = 0.06$  W/mK  
 $\Psi = 0.12$  W/mK

# Closing the Loop

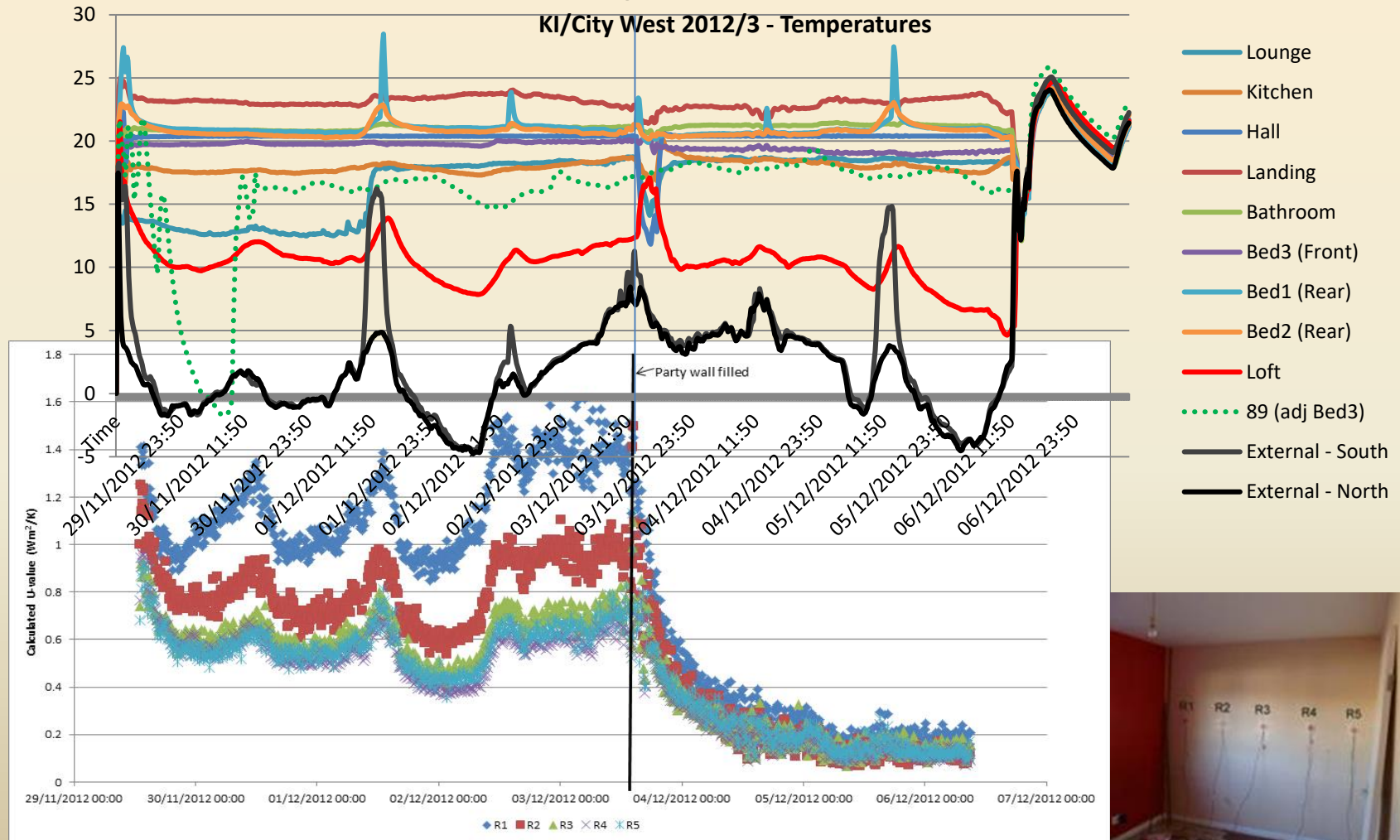
Designed HLC 134.9 W/K - Measured HLC 220.6 W/K



# Simple Tests



# Simple Tests

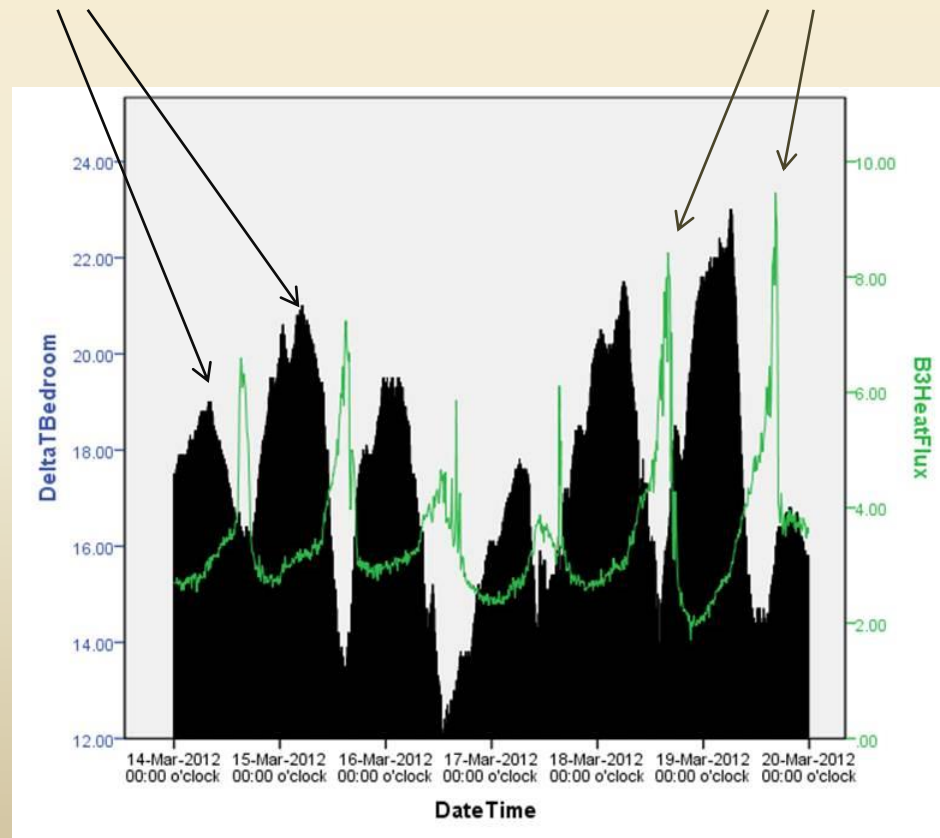




# Simple Test Issues: Thermal Lag

Maximum  $\Delta T$

Maximum Heat Flux





## Whole House Heat Loss Test Method (Coheating)

Dr David Johnston, Centre for the Built Environment, Leeds Metropolitan University  
Dominic Miles-Shenton, Centre for the Built Environment, Leeds Metropolitan University  
Dr Jez Wingfield, Willmott Dixon Energy Services Limited  
David Farmer, Centre for the Built Environment, Leeds Metropolitan University  
Prof Malcolm Bell, Centre for the Built Environment, Leeds Metropolitan University

March – 2012

<http://www.leedsmet.ac.uk/as/cebe/index.htm>



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